

Measuring 21cm global spectrum on the lunar orbit

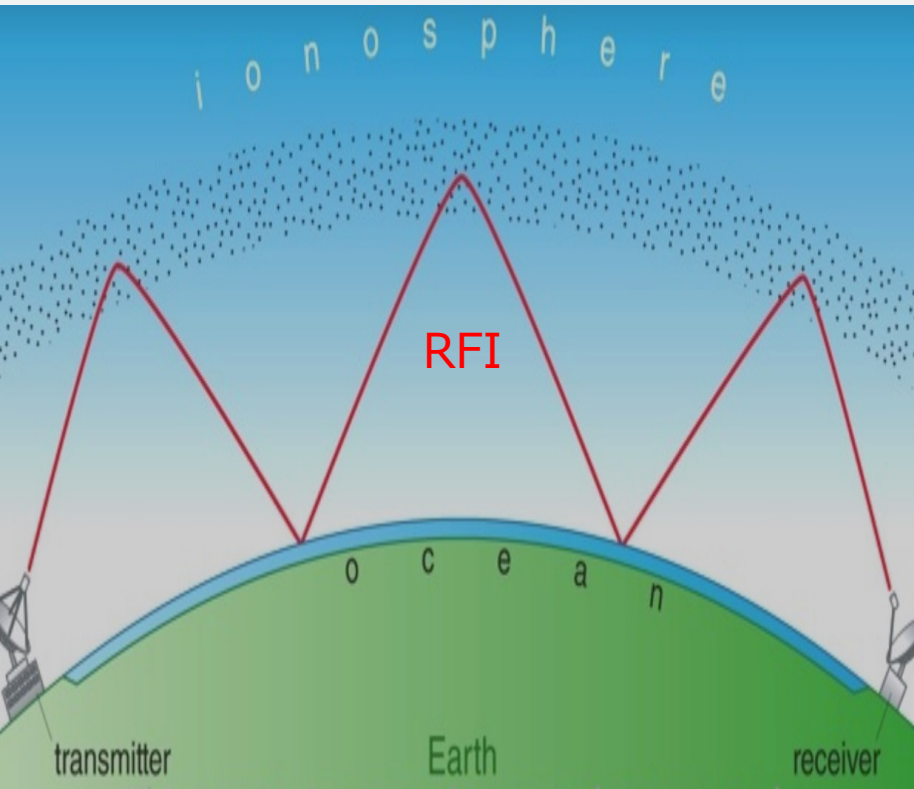
---High-frequency payload in Hongmeng project

Fengquan Wu
Payload development team
NAOC

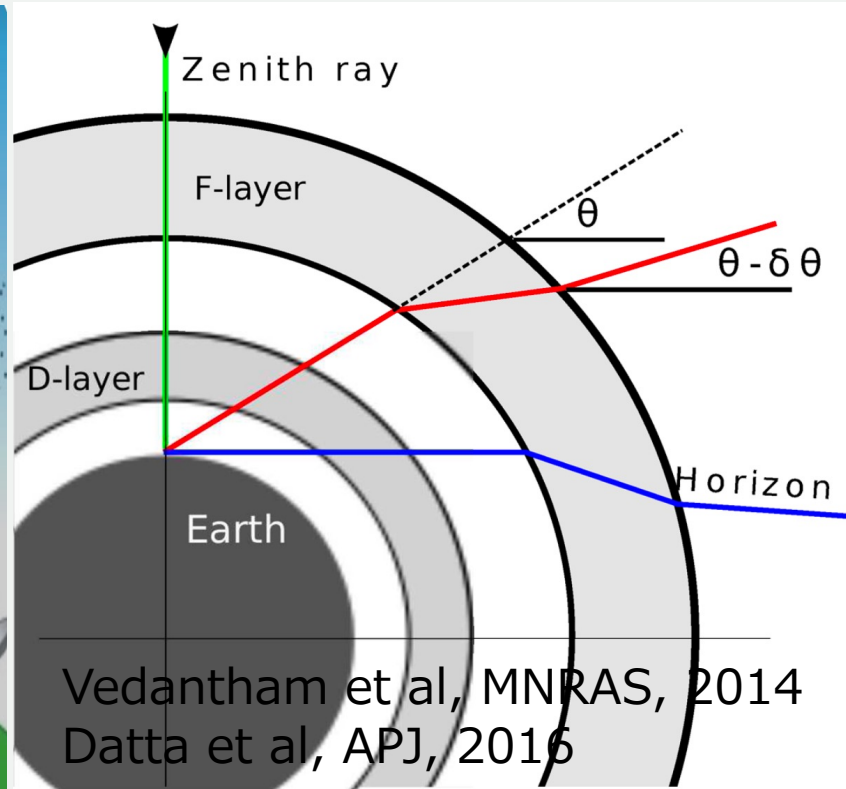
21 cm Cosmology Workshop 2024
Hangzhou July 23



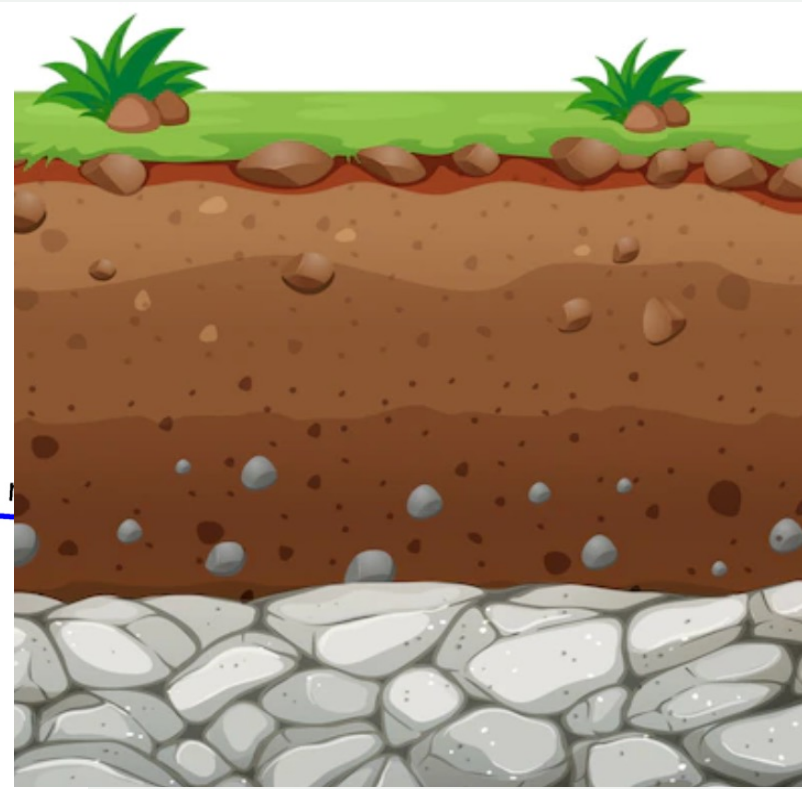
21cm global spectrum – Environment effect



RFI contamination



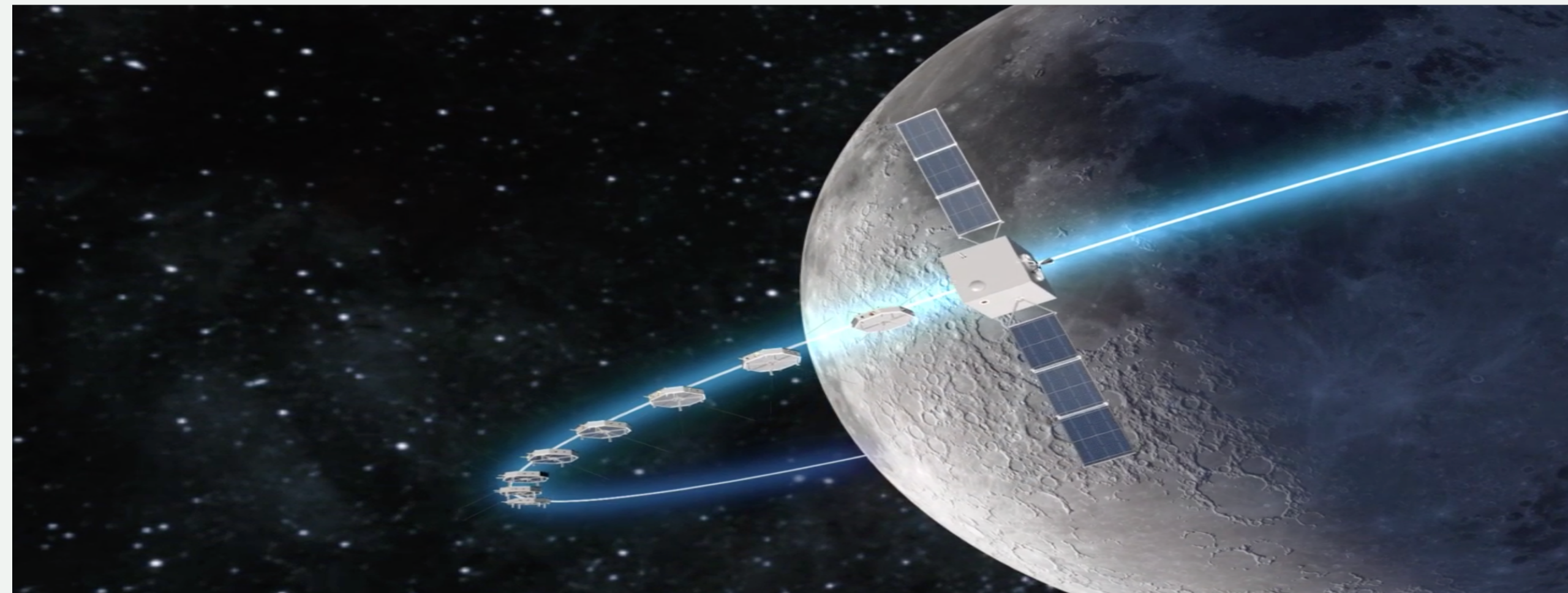
Ionosphere effect



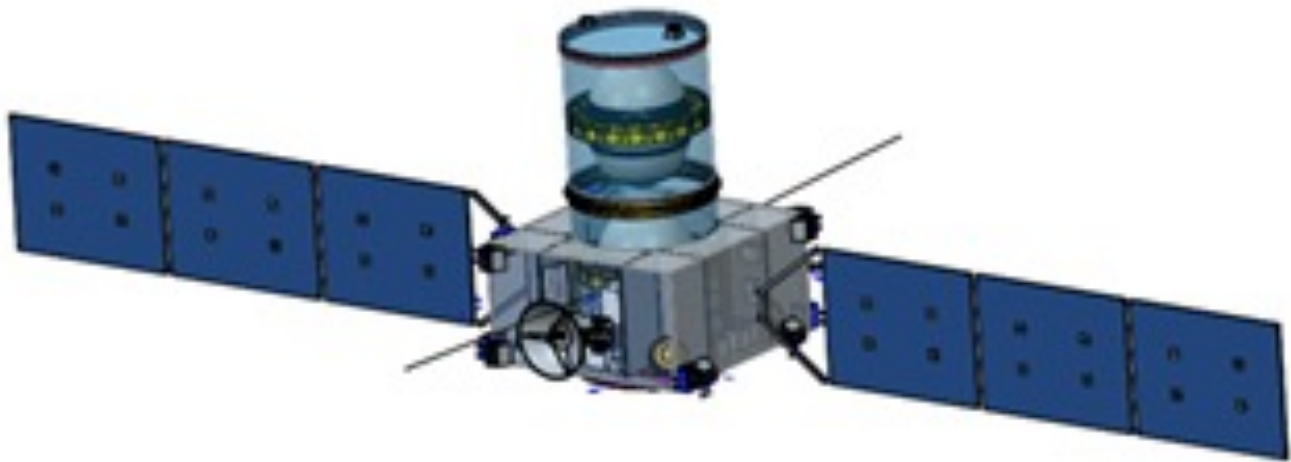
Ground effect

Overview of Hongmeng (鸿蒙) project (PI: Xuelel Chen)

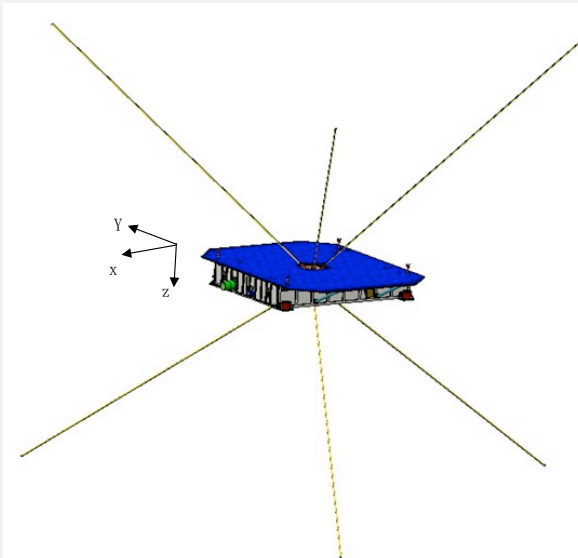
Long wavelength array on lunar orbit (Pre-study project in CAS)



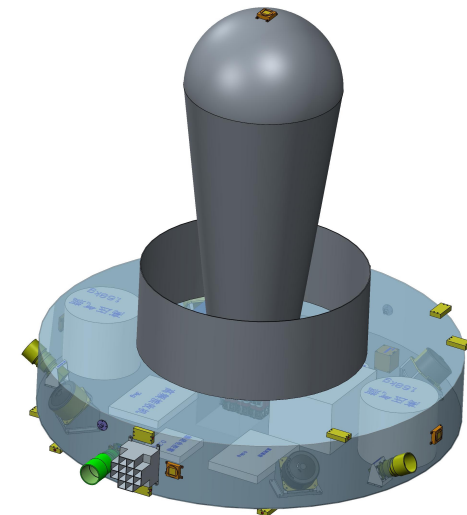
- Whole sky imaging at frequency below 30MHz
- Global spectrum measurement at frequency below 120MHz



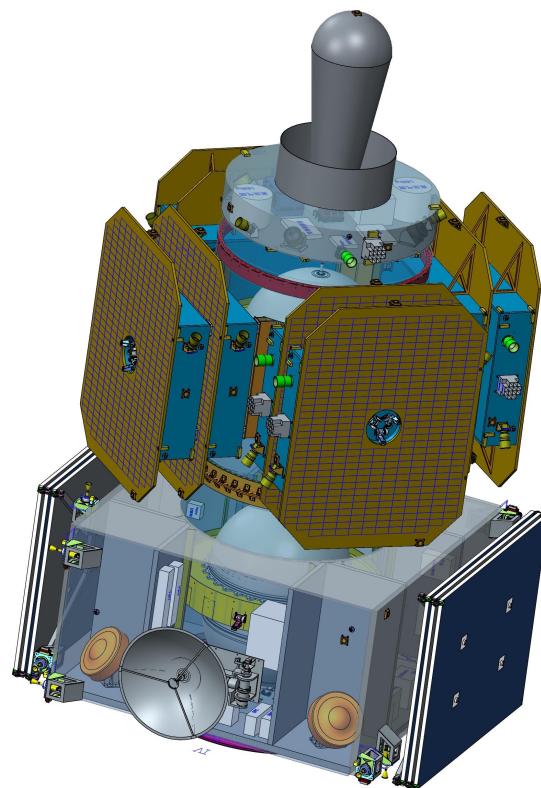
600kg



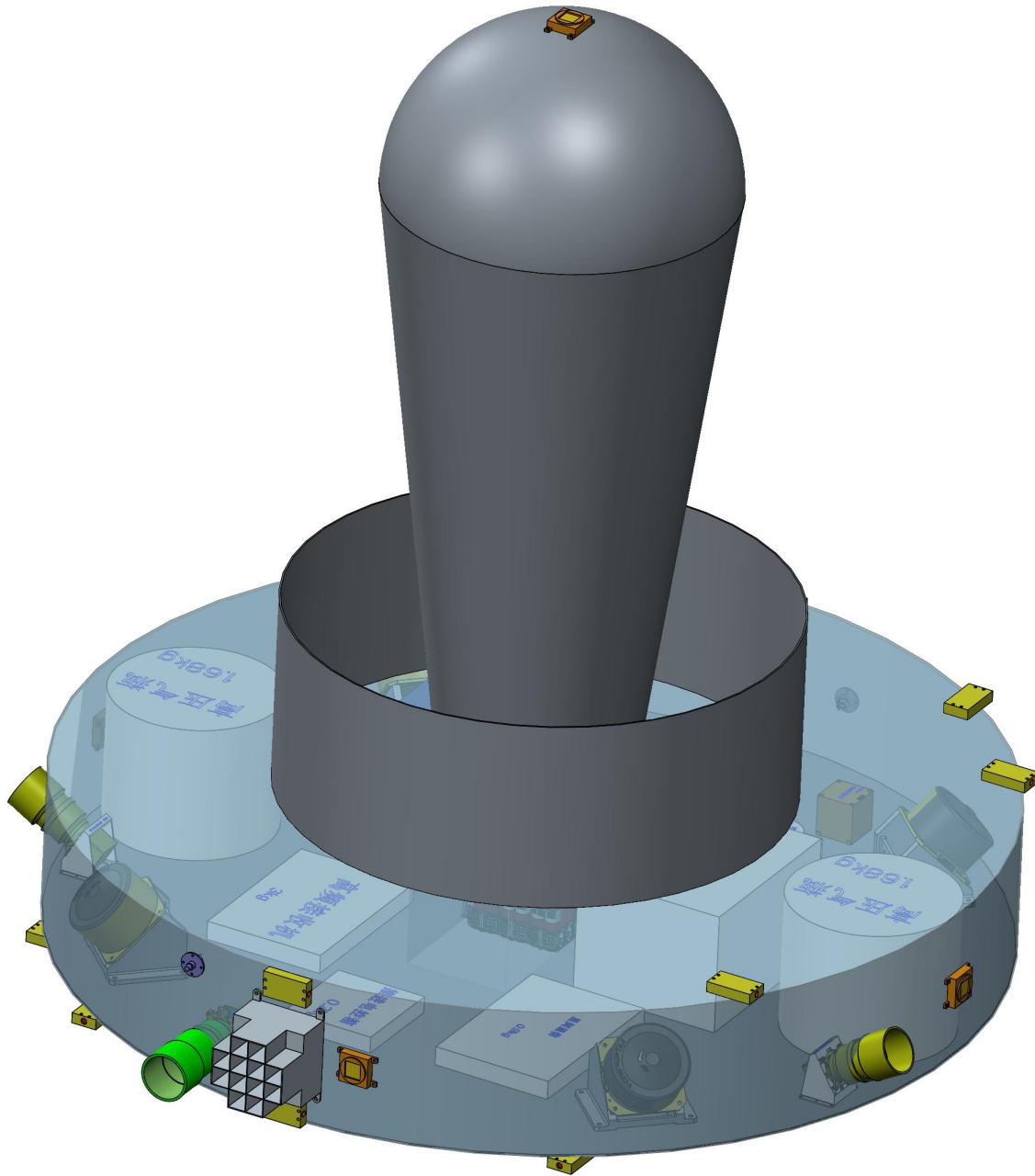
80kg



90kg



1300kg

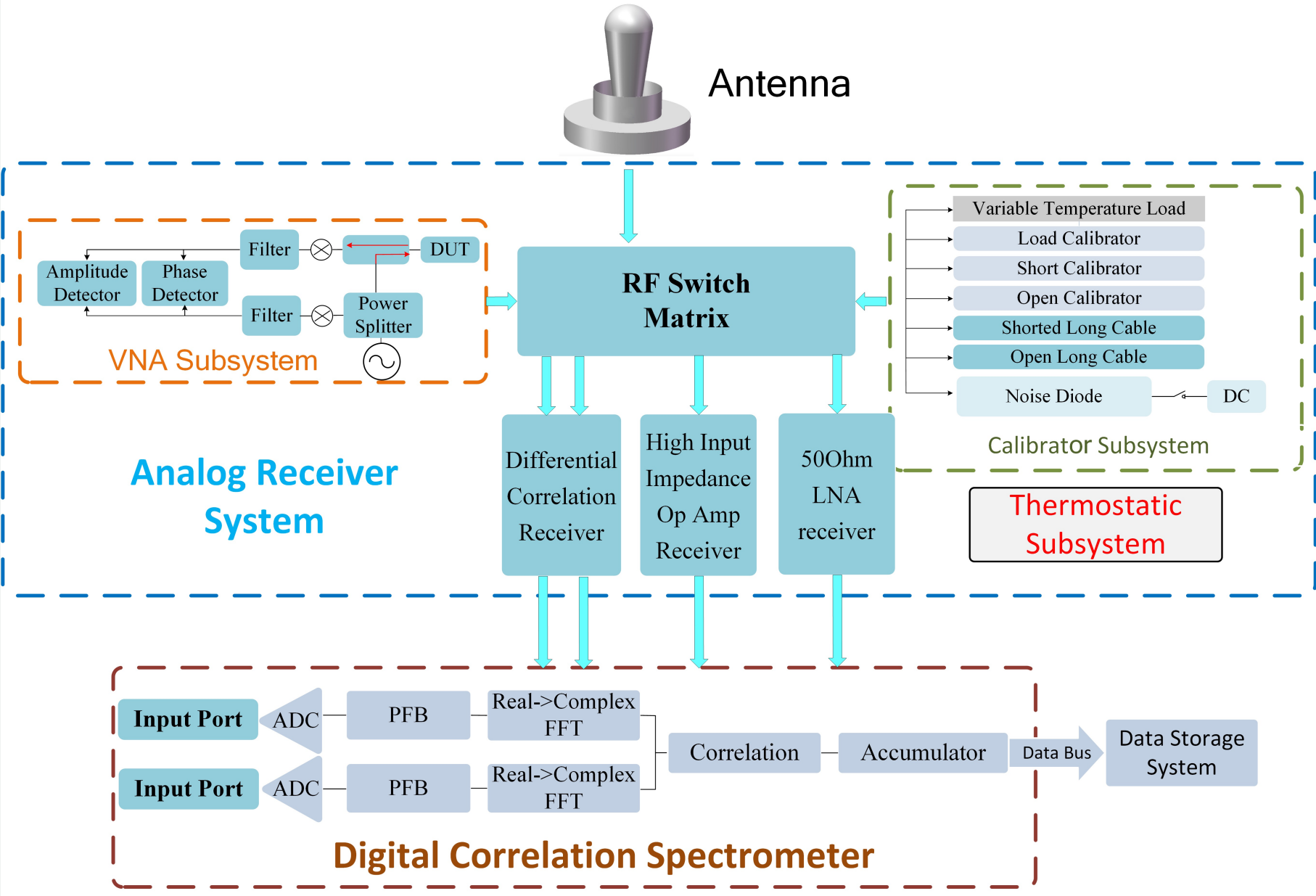


Antenna

Loaded ring

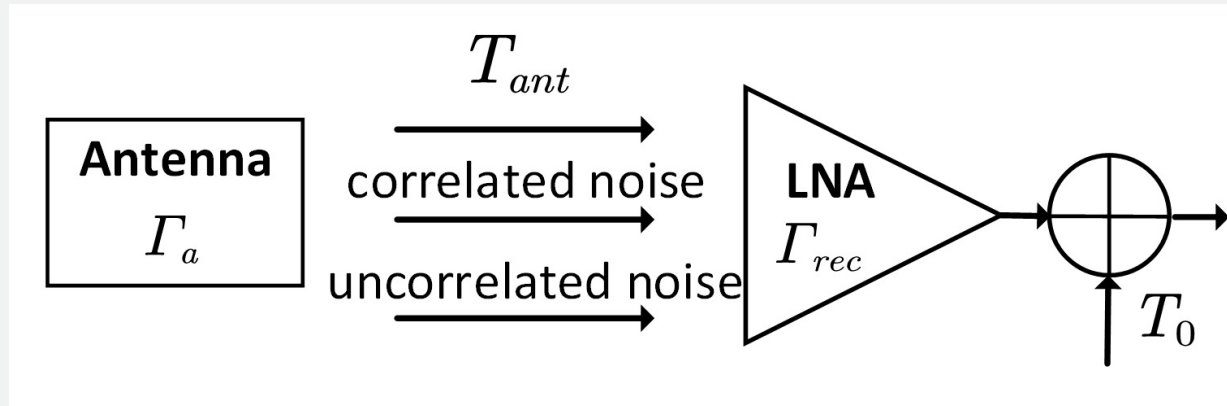
Satellite body

System design of global spectrum satellite



Multi-receiver design :
Cross check the system effect and signal

Two-port noise wave for 50 Ohm LNA receiver



$$X_{unc} = -\frac{|\Gamma_{cal}|^2}{1 - |\Gamma_{cal}|^2},$$

$$X_L = \frac{|1 - \Gamma_{cal}\Gamma_{rec}|^2}{1 - |\Gamma_{cal}|^2},$$

$$X_{cos} = -\text{Re} \left(\frac{\Gamma_{cal}}{1 - \Gamma_{cal}\Gamma_{rec}} \times \frac{X_L}{\sqrt{1 - |\Gamma_{rec}|^2}} \right),$$

$$X_{sin} = -\text{Im} \left(\frac{\Gamma_{cal}}{1 - \Gamma_{cal}\Gamma_{rec}} \times \frac{X_L}{\sqrt{1 - |\Gamma_{rec}|^2}} \right),$$

$$X_{NS} = \left(\frac{P_{cal} - P_L}{P_{NS} - P_L} \right) X_L,$$

$$X_{unc}T_{unc} + X_{cos}T_{cos} + X_{sin}T_{sin} + X_{NS}T_{NS} + X_L T_L = T_{cal}$$

Use 5 calibrators to solve for noise parameters at each frequency point

Four-port noise wave for differential receiver

The whole system can be modelled as a **four-port microwave network**

Consider the case where the **antenna** connected to port 1 is a temperature source and the other ports are only involved in signal reflection.

$$T_1(V_1) = \frac{|V_1|^2}{8Z_0} \frac{|1 - \Gamma_1|^2}{(1 - |\Gamma_1|^2)} \quad V_1^+(V_1) = \frac{V_1(1 - \Gamma_1)}{2(1 - \Gamma_1\Gamma_{in1})} \quad \Gamma_{in1} = V_1^-/V_1^+$$

$$\begin{bmatrix} V_1^- \\ V_2^- \\ V_3^- \\ V_4^- \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} & S_{13} & S_{14} \\ S_{21} & S_{22} & S_{23} & S_{24} \\ S_{31} & S_{32} & S_{33} & S_{34} \\ S_{41} & S_{42} & S_{43} & S_{44} \end{bmatrix} \begin{bmatrix} V_1^+ \\ V_2^+ \\ V_3^+ \\ V_4^+ \end{bmatrix} \quad \begin{aligned} \Gamma_2 &= V_2^+/V_2^- \\ \Gamma_3 &= V_3^+/V_3^- \\ \Gamma_4 &= V_4^+/V_4^- \end{aligned}$$

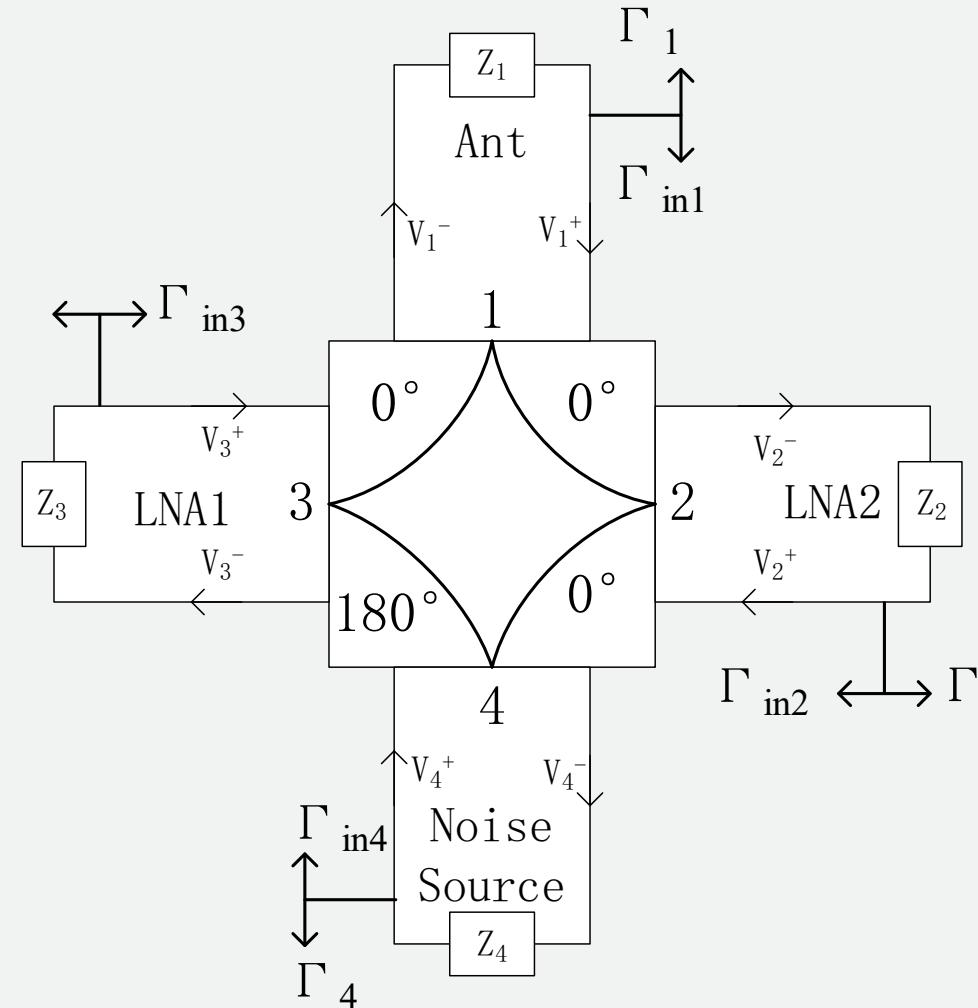
With the equation above, we can obtain all V_i^- and V_i^+ with respect to T_1 , the equivalent temperature of antenna.

The cross-correlation power is $P_c = \frac{V_{20}^* V_{30}}{2Z_0}$, with

$$V_{20} = G_2 V_2^- \sqrt{(1 - |\Gamma_2|^2)}$$

$$V_{30} = G_3 V_3^- \sqrt{(1 - |\Gamma_3|^2)}$$

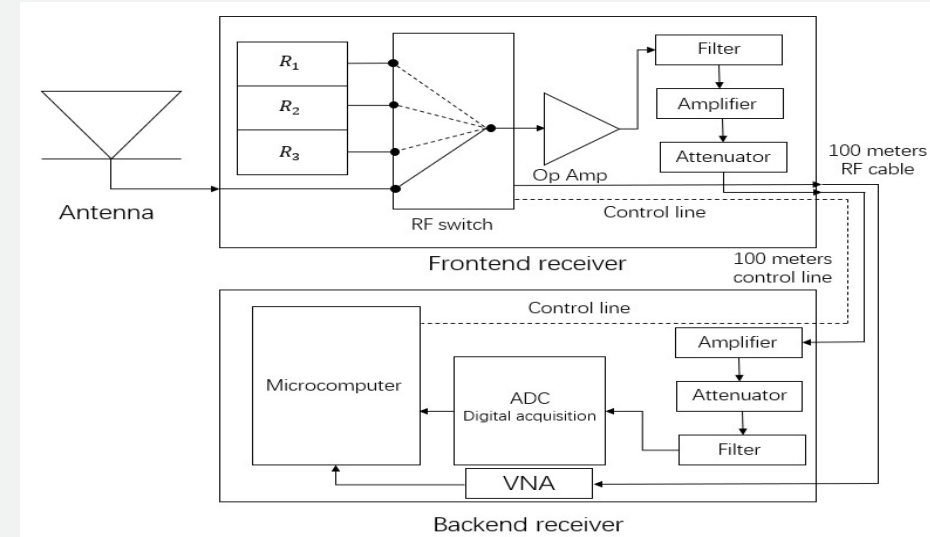
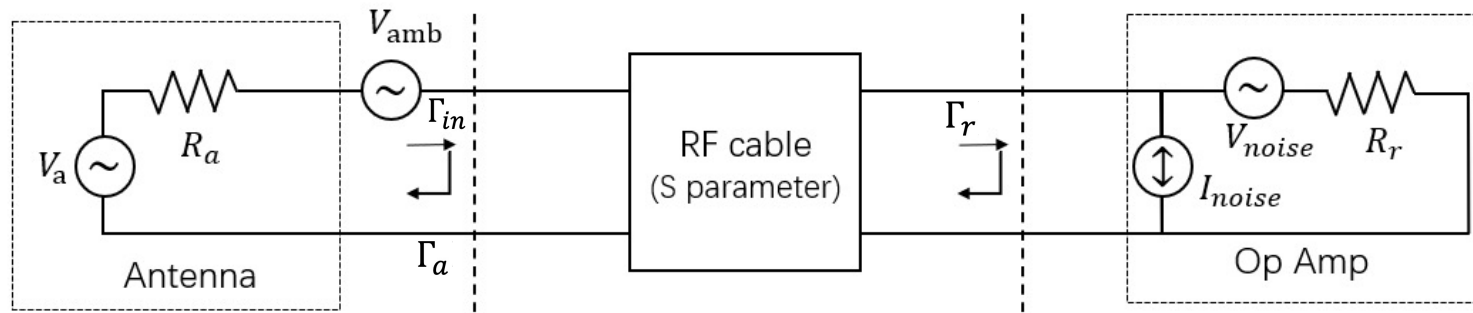
Similarly, we can calculate cross-correlation power generated by **noise source** and **uncorrelated part of two LNAs noise**.



Multi-resistor calibration for high impedance receiver

$$P = g[(4R_aKT + |V_{amb}|^2) |S_0|^2 + I_{noise}^2 Z^2 + V_{noise}^2]$$

$$S_0 = \frac{Z_0}{Z_a + Z_0} \frac{e^{-\gamma l}(1 + \Gamma_r)}{(1 - S_{22}\Gamma_r)(1 - \Gamma_a\Gamma_{in})}$$



Simulation & Error propagation analysis

Calibration Error in 21-centimeter Global Spectrum Experiments

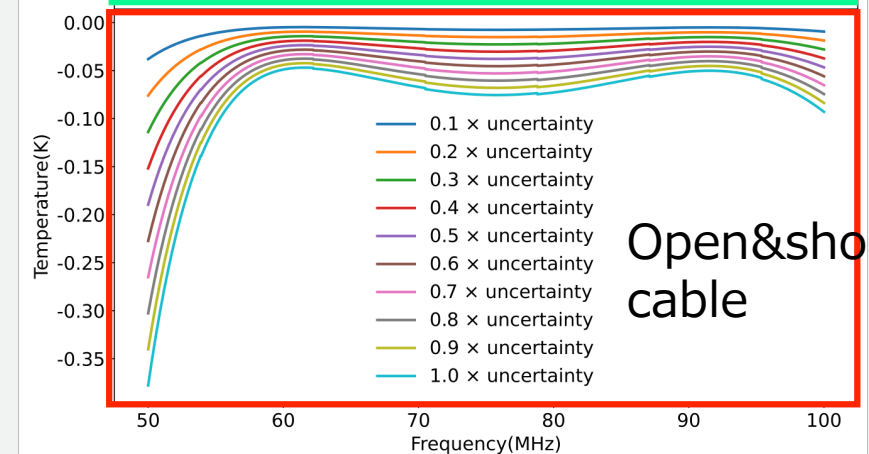
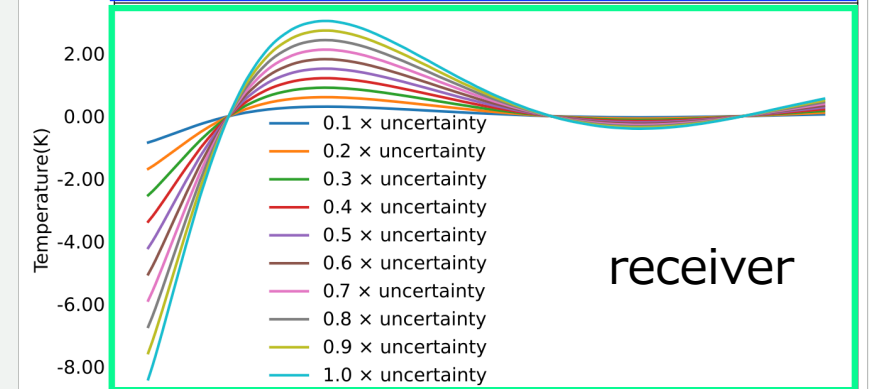
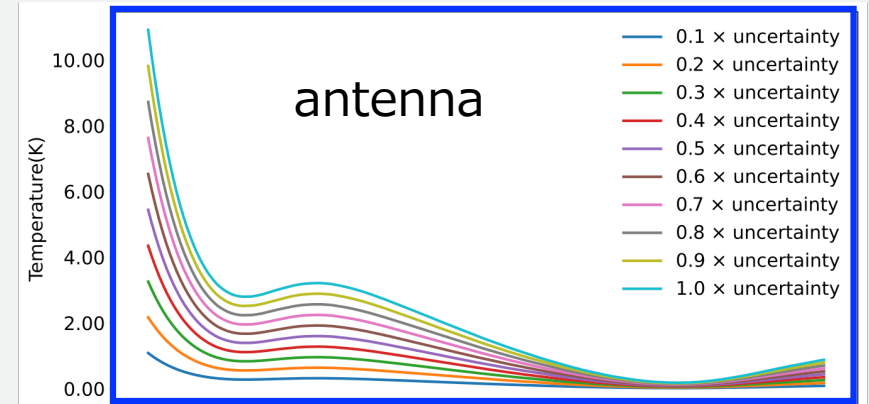
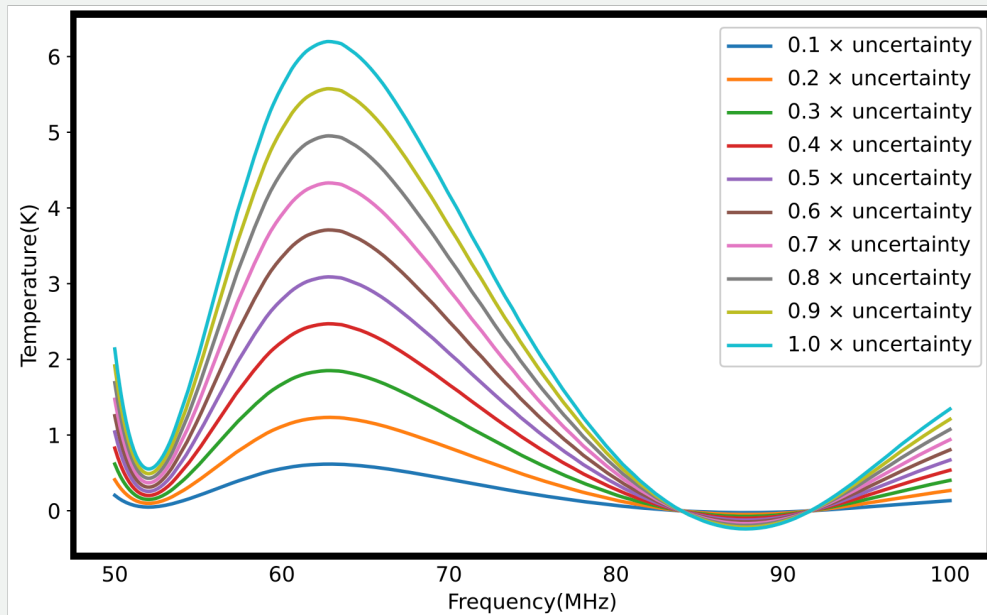
Shijie Sun et.al. Universe 2024, 10(6), 236

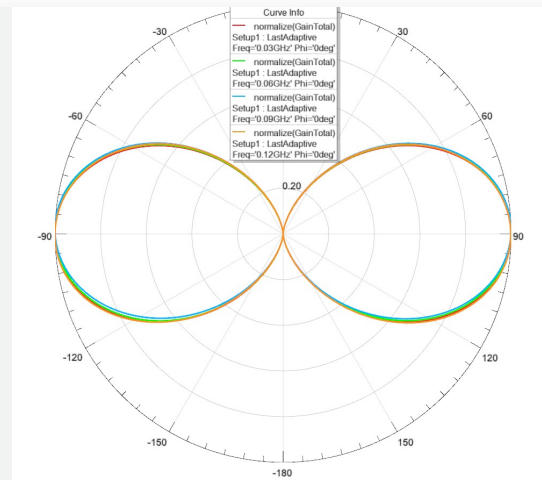
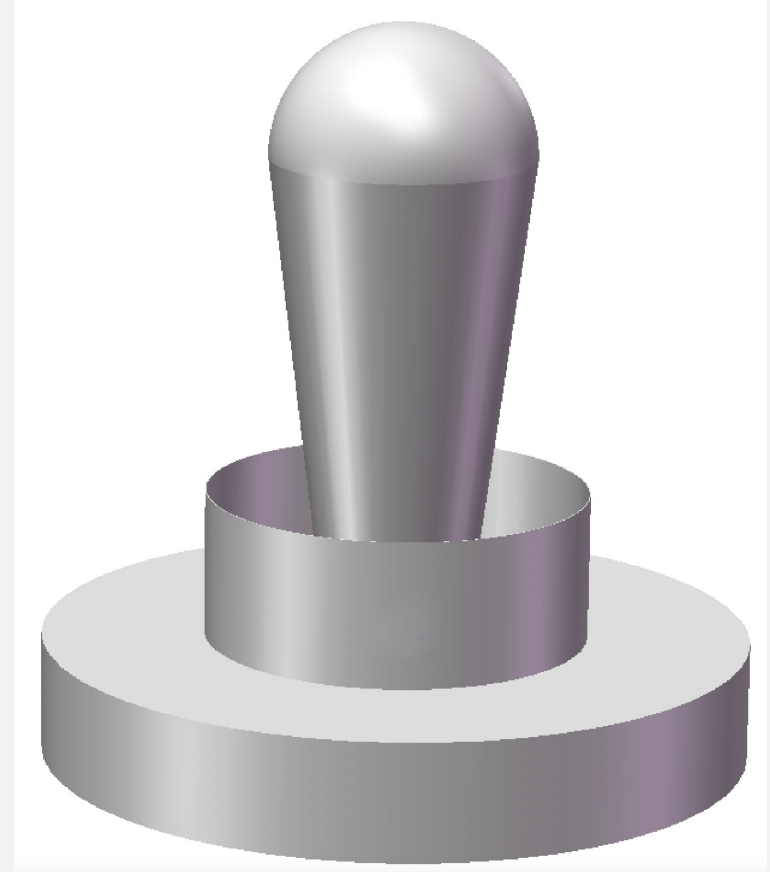
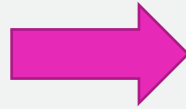
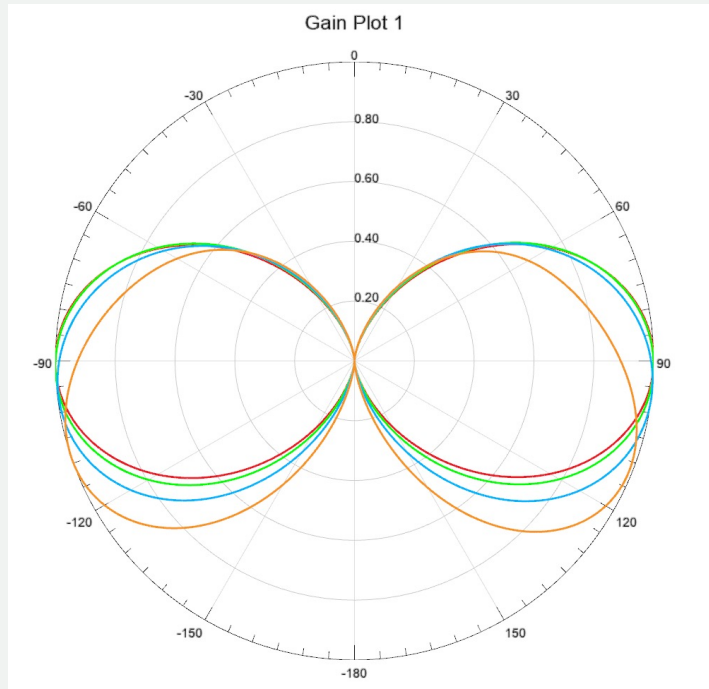
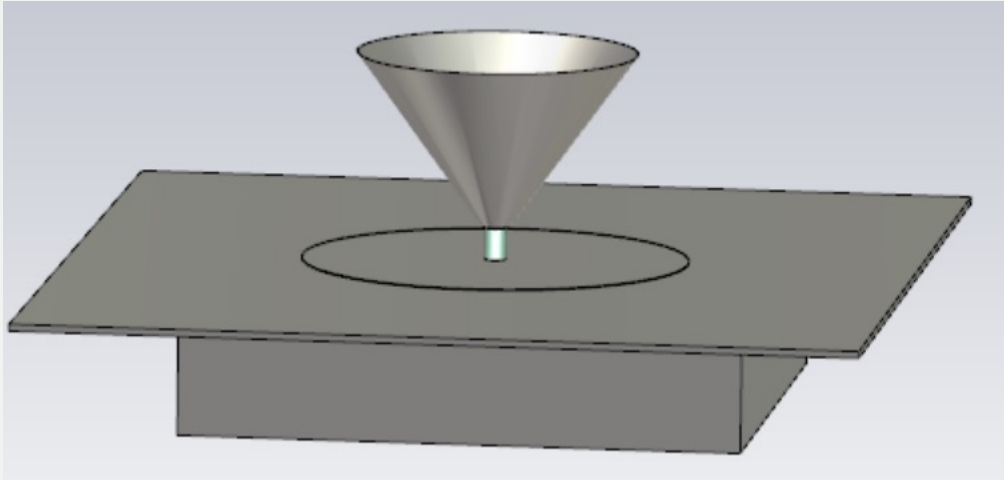
$$T_{\text{sky}} = \frac{T_{\text{ant}} - T_0}{(1 - |\Gamma_{\text{ant}}|^2)|F_{\text{ant}}|^2} - \frac{T_u |\Gamma_{\text{ant}}|^2}{1 - |\Gamma_{\text{ant}}|^2} - \frac{(T_c \cos(\phi) + T_s \sin(\phi)) |\Gamma_{\text{ant}}|}{(1 - |\Gamma_{\text{ant}}|^2)|F_{\text{ant}}|} \quad F_{\text{ant}} = \frac{(1 - |\Gamma_{\text{rec}}|^2)^{\frac{1}{2}}}{1 - \Gamma_{\text{ant}}\Gamma_{\text{rec}}}$$

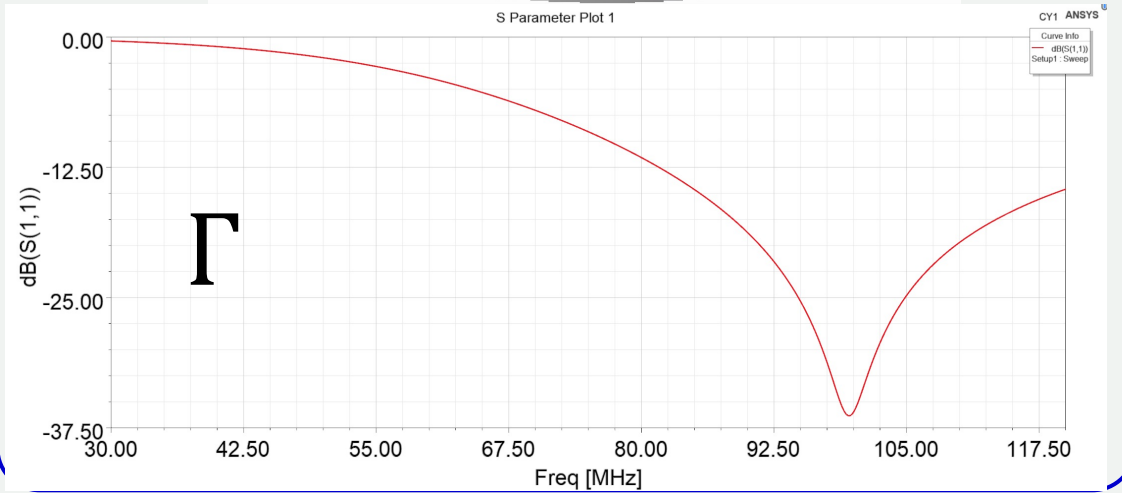
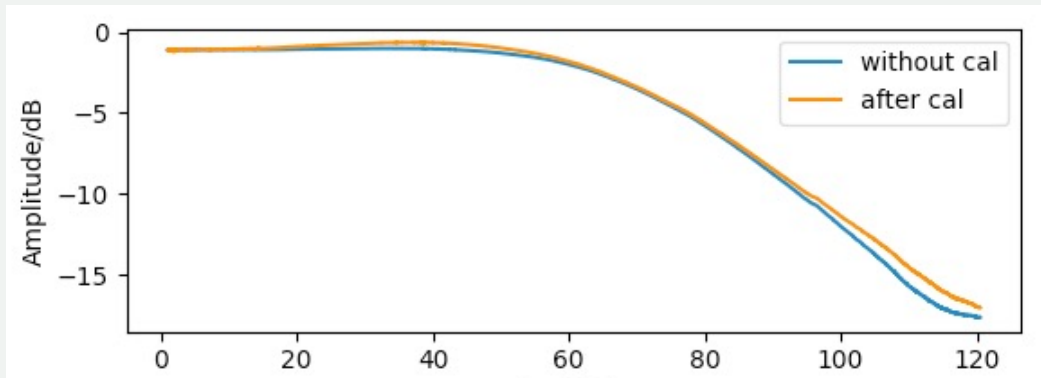
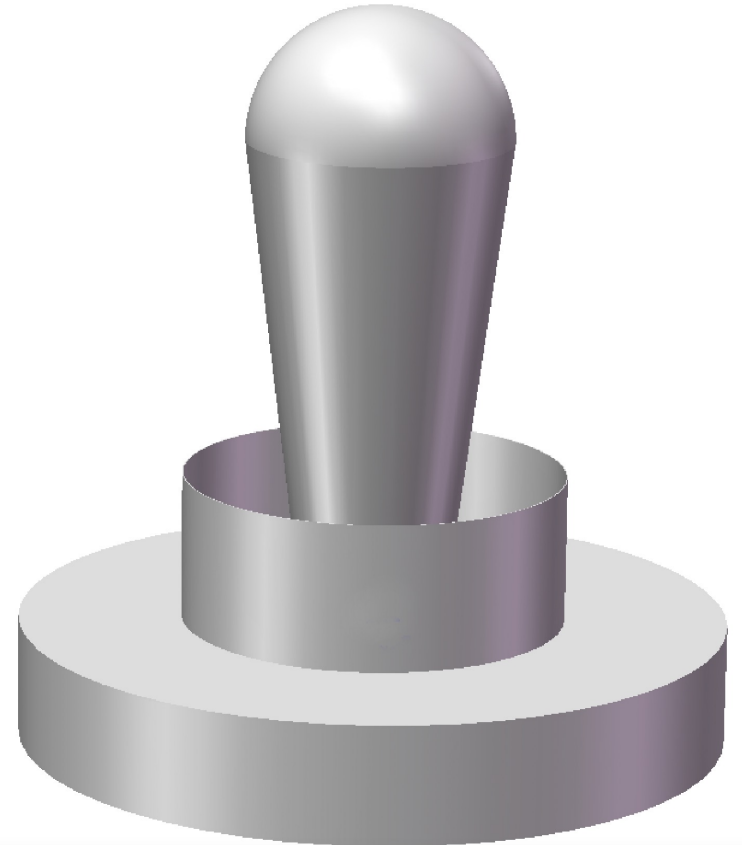
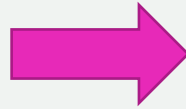
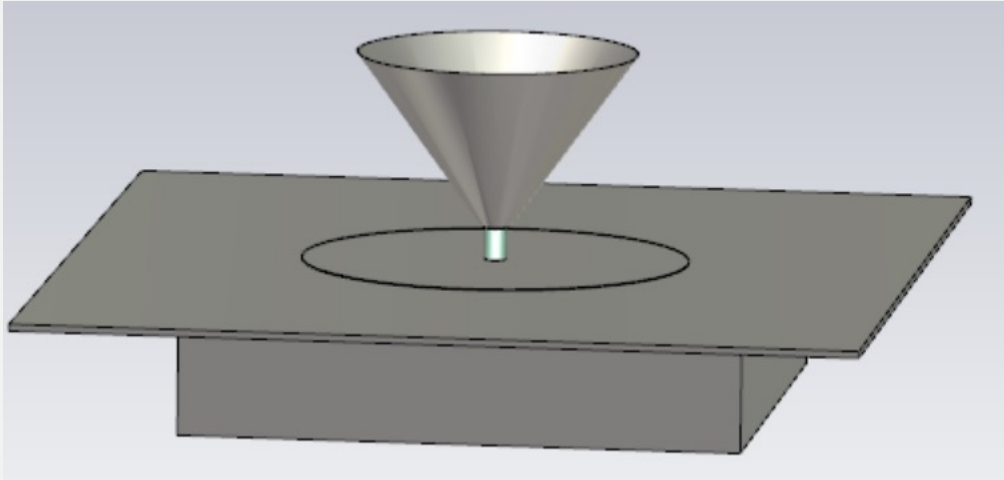
$$\delta T_{\text{sky}} = \frac{\partial T_{\text{sky}}}{\partial \Gamma_{\text{ant}}} \delta \Gamma_{\text{ant}} + \frac{\partial T_{\text{sky}}}{\partial \Gamma_{\text{rec}}} \delta \Gamma_{\text{rec}} + \frac{\partial T_{\text{sky}}}{\partial \Gamma_{\text{open}}} \delta \Gamma_{\text{open}}$$

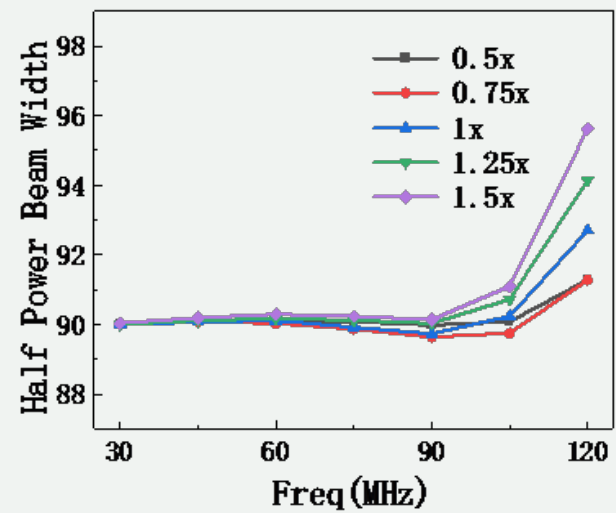
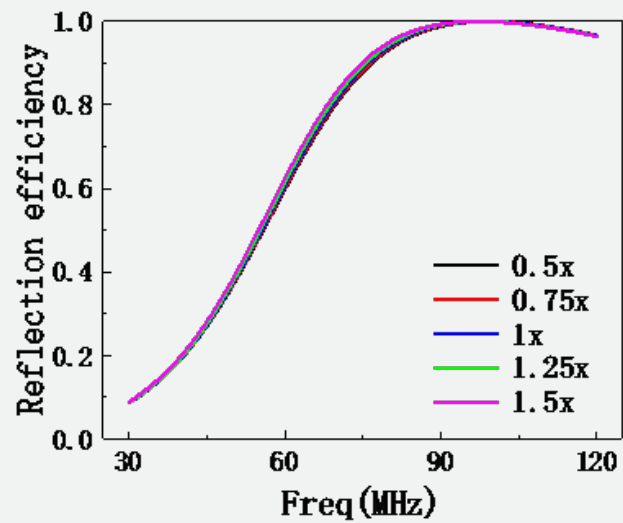
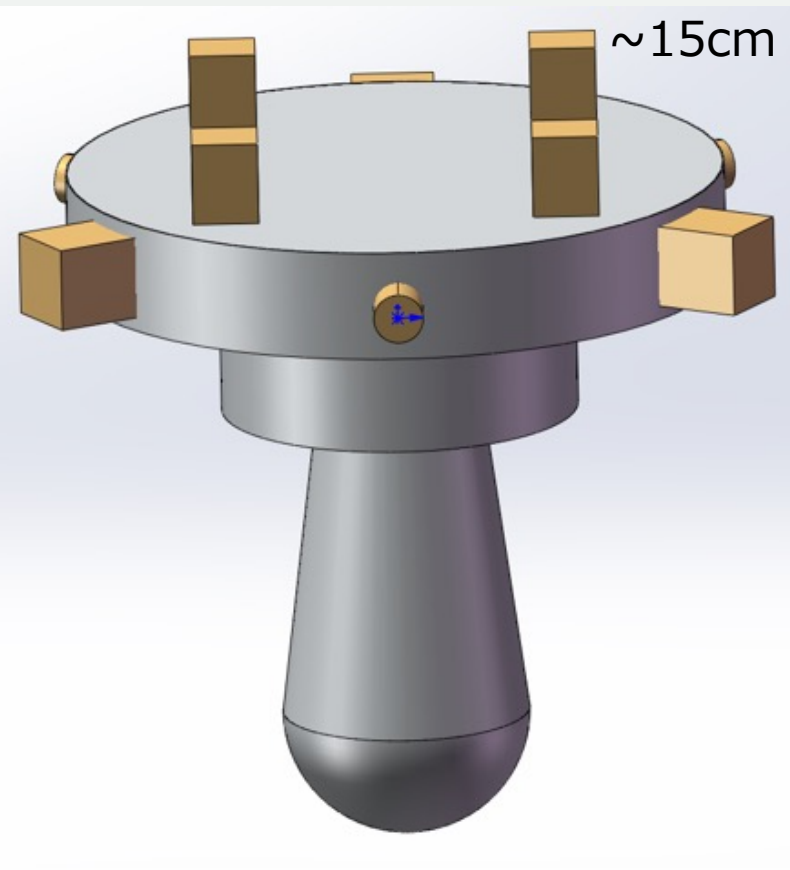
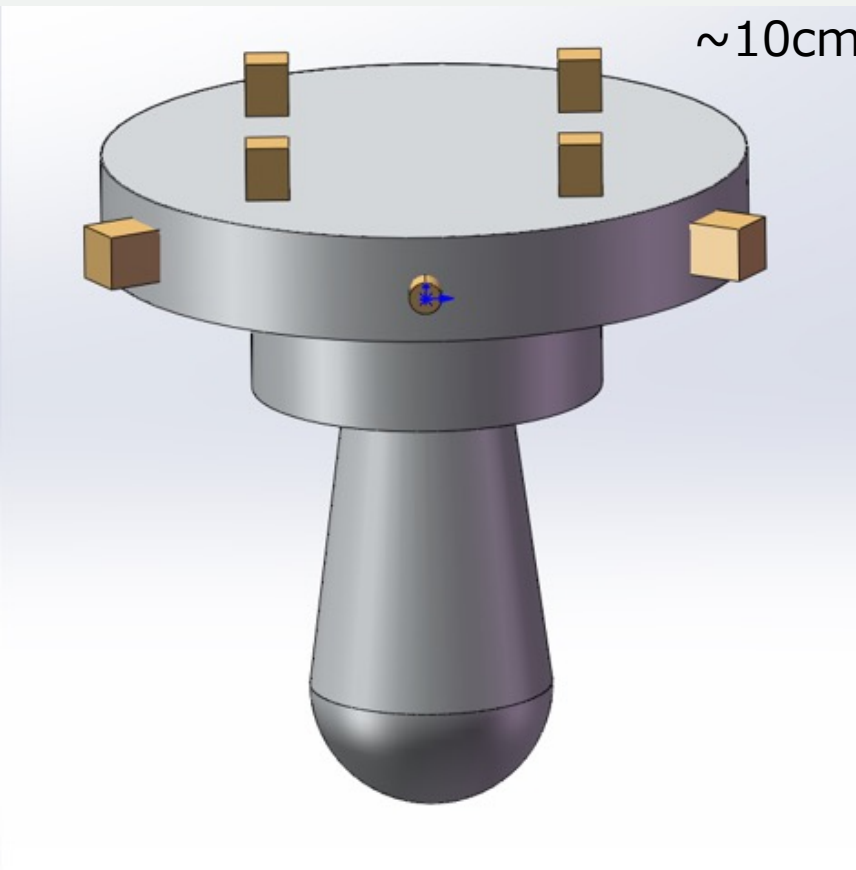
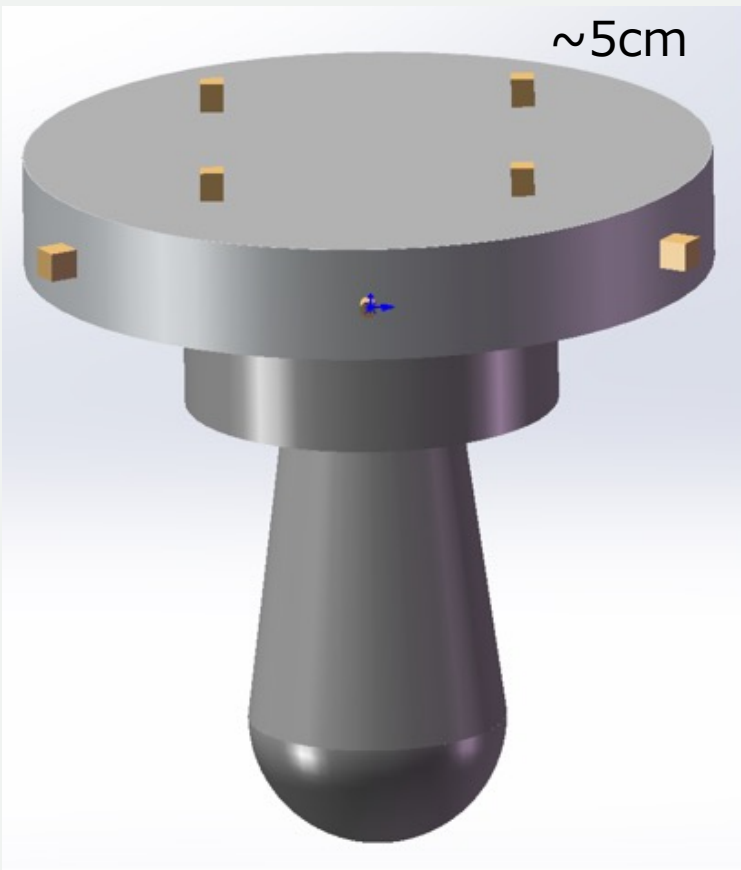
$$\frac{\partial T_{\text{sky}}}{\partial \Gamma_{\text{open}}} = \frac{\partial T_{\text{sky}}}{\partial T_u} \frac{\partial T_u}{\partial \Gamma_{\text{open}}} + \frac{\partial T_{\text{sky}}}{\partial T_c} \frac{\partial T_c}{\partial \Gamma_{\text{open}}} + \frac{\partial T_{\text{sky}}}{\partial T_s} \frac{\partial T_s}{\partial \Gamma_{\text{open}}}$$

$$\frac{\partial T_{\text{sky}}}{\partial \Gamma_{\text{rec}}} = \frac{\partial T_{\text{sky}}}{\partial \Gamma_{\text{rec}}} \Big|_{\text{direct}} + \frac{\partial T_{\text{sky}}}{\partial T_u} \frac{\partial T_u}{\partial \Gamma_{\text{rec}}} + \frac{\partial T_{\text{sky}}}{\partial T_c} \frac{\partial T_c}{\partial \Gamma_{\text{rec}}} + \frac{\partial T_{\text{sky}}}{\partial T_s} \frac{\partial T_s}{\partial \Gamma_{\text{rec}}} + \frac{\partial T_{\text{sky}}}{\partial T_0} \frac{\partial T_0}{\partial \Gamma_{\text{rec}}}$$







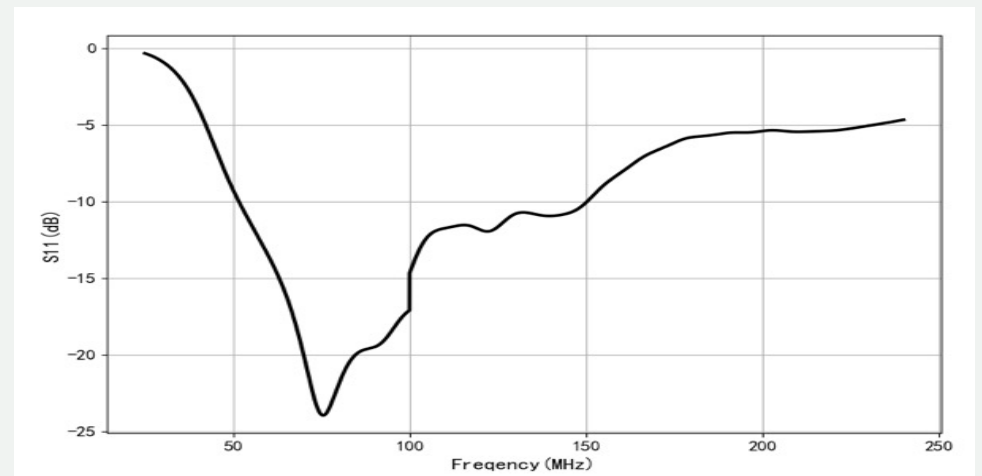
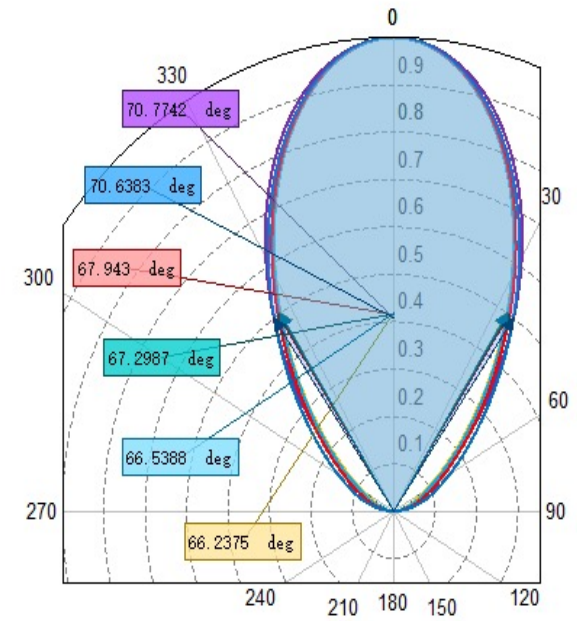
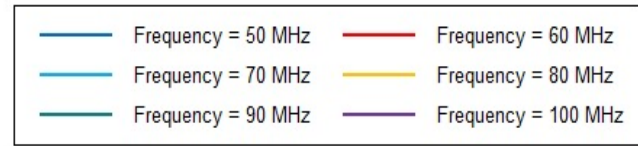




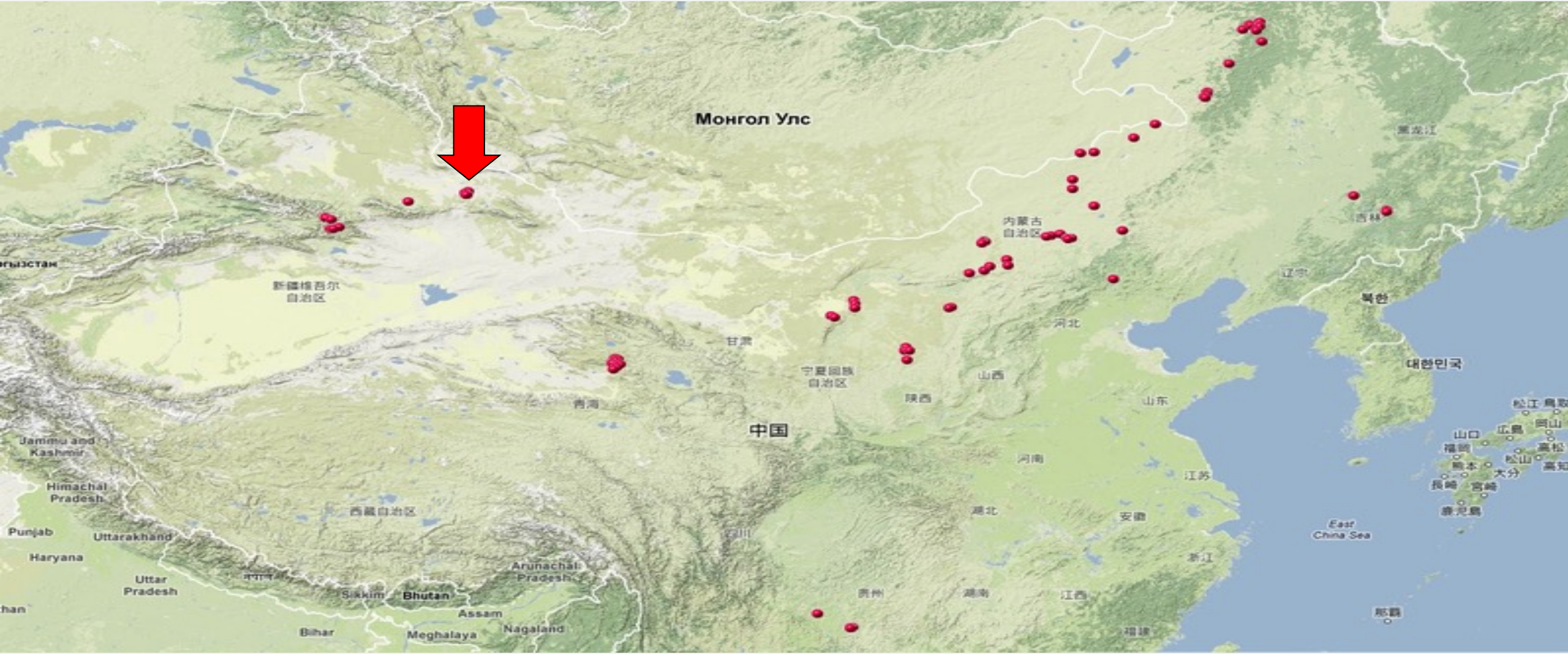
Testing of 50 Ohm LNA receiver channel



Far field



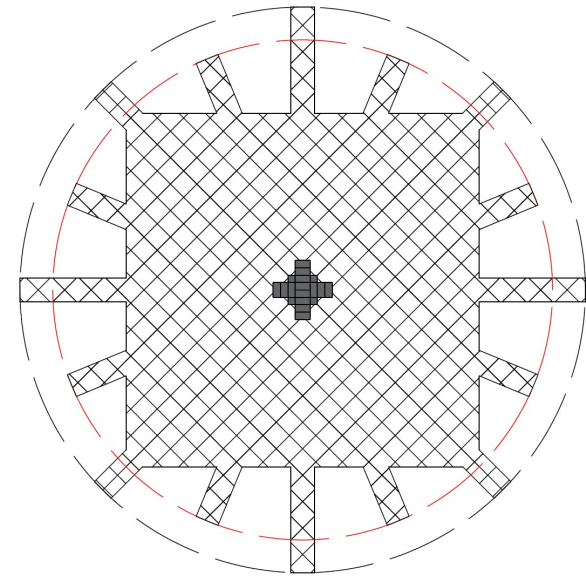
Field Testing Site in Xinjiang



Tianlai array (天籟阵列) ---Radio interferometer array for dark energy



Field Testing in Xinjiang

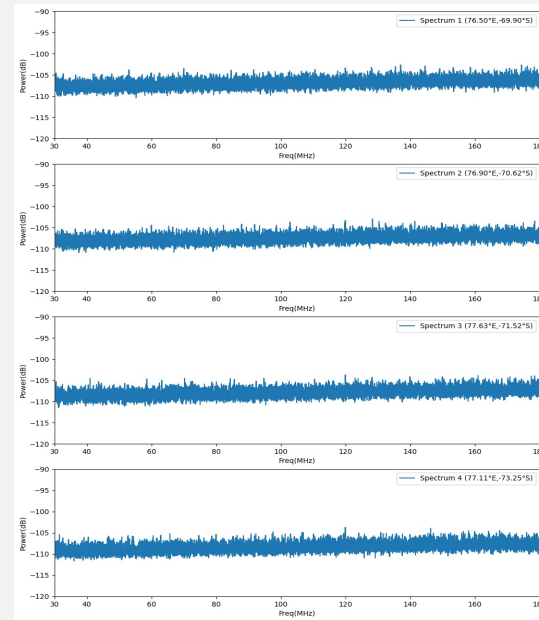
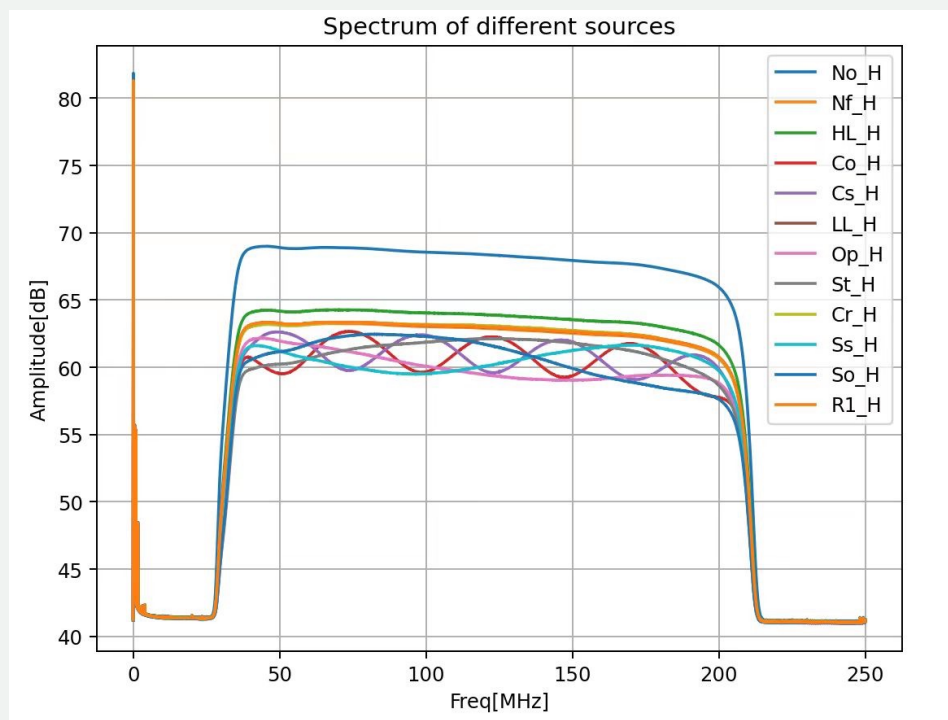


Ground plate

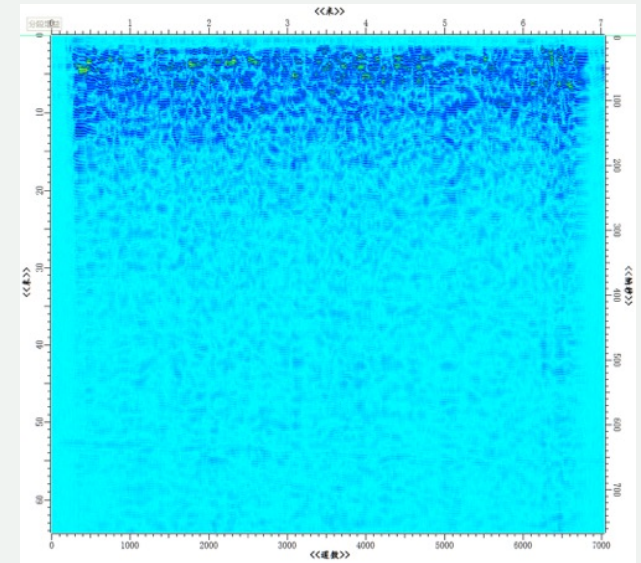
Field Testing in Antarctica



Architecture on The Big Ice

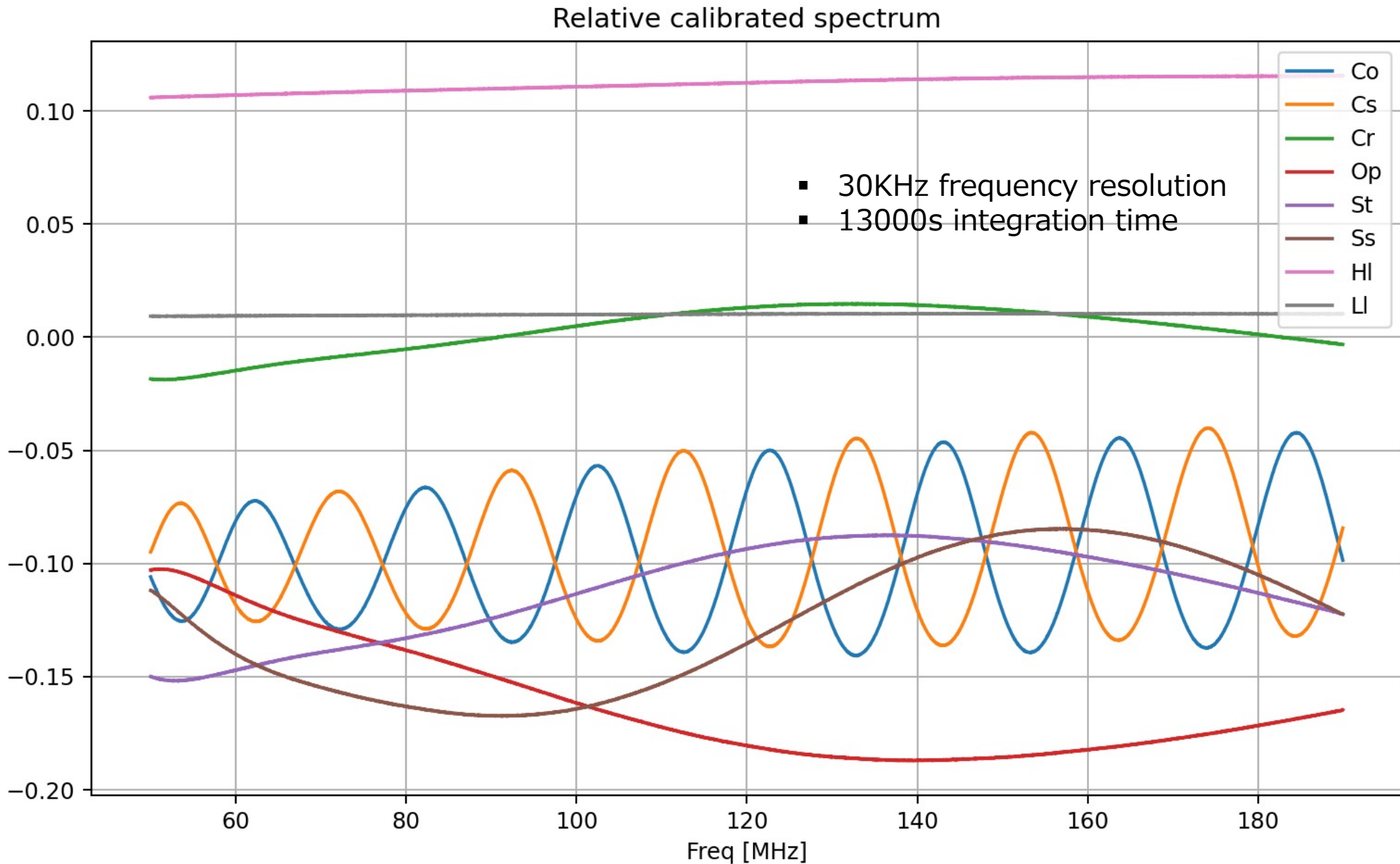


RF environment

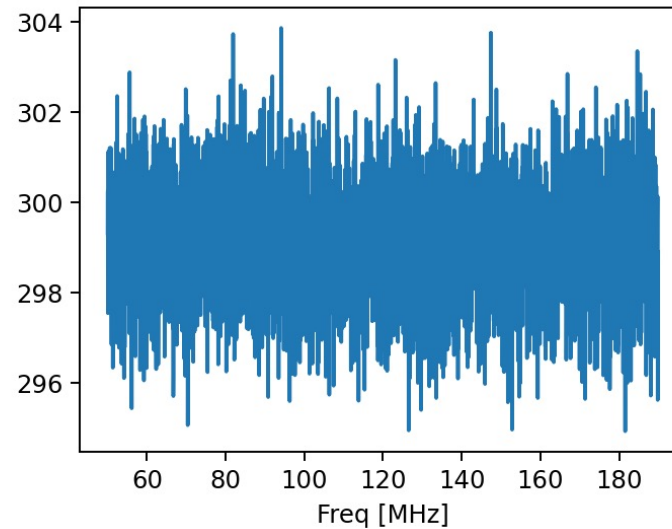
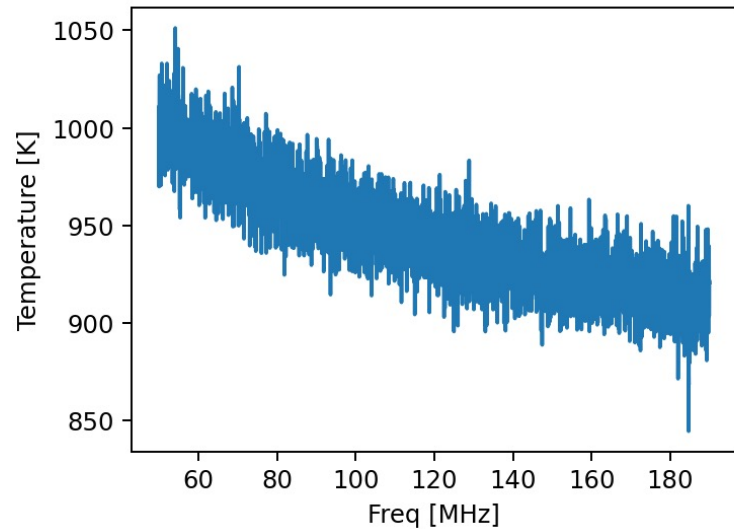
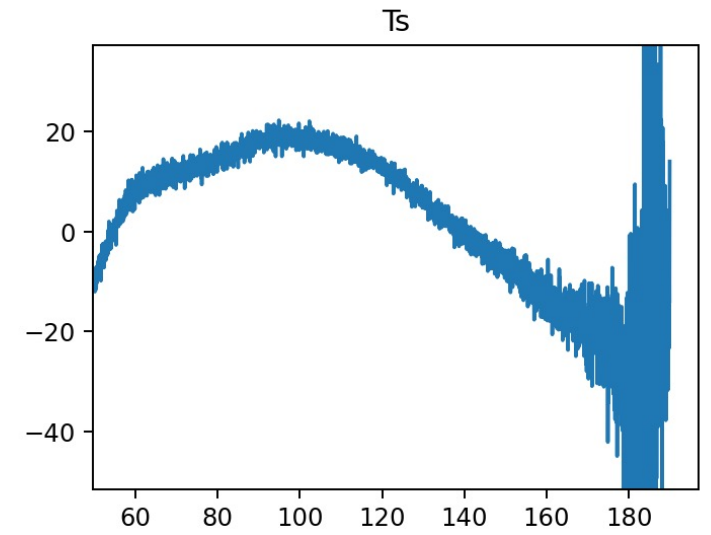
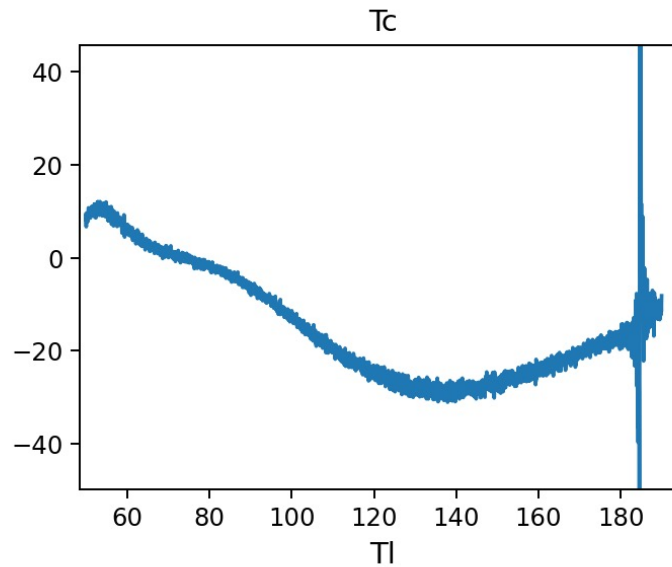
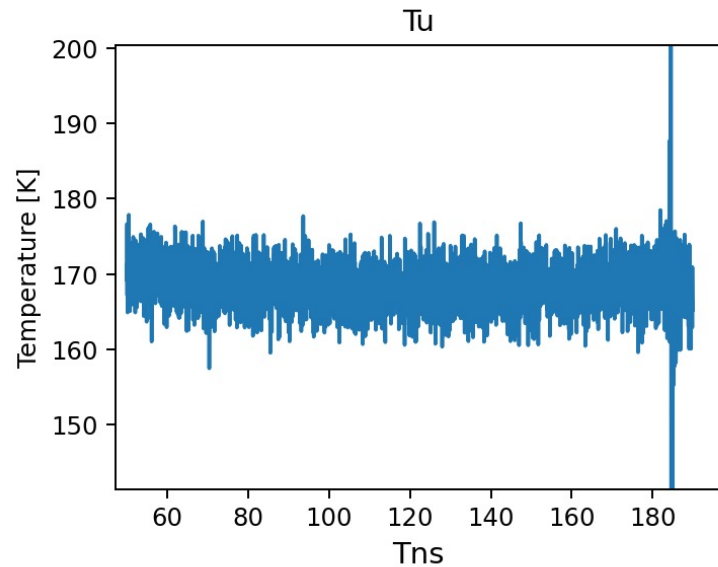


Ground penetrating radar

Spectra after Relative calibration



Noise wave parameters



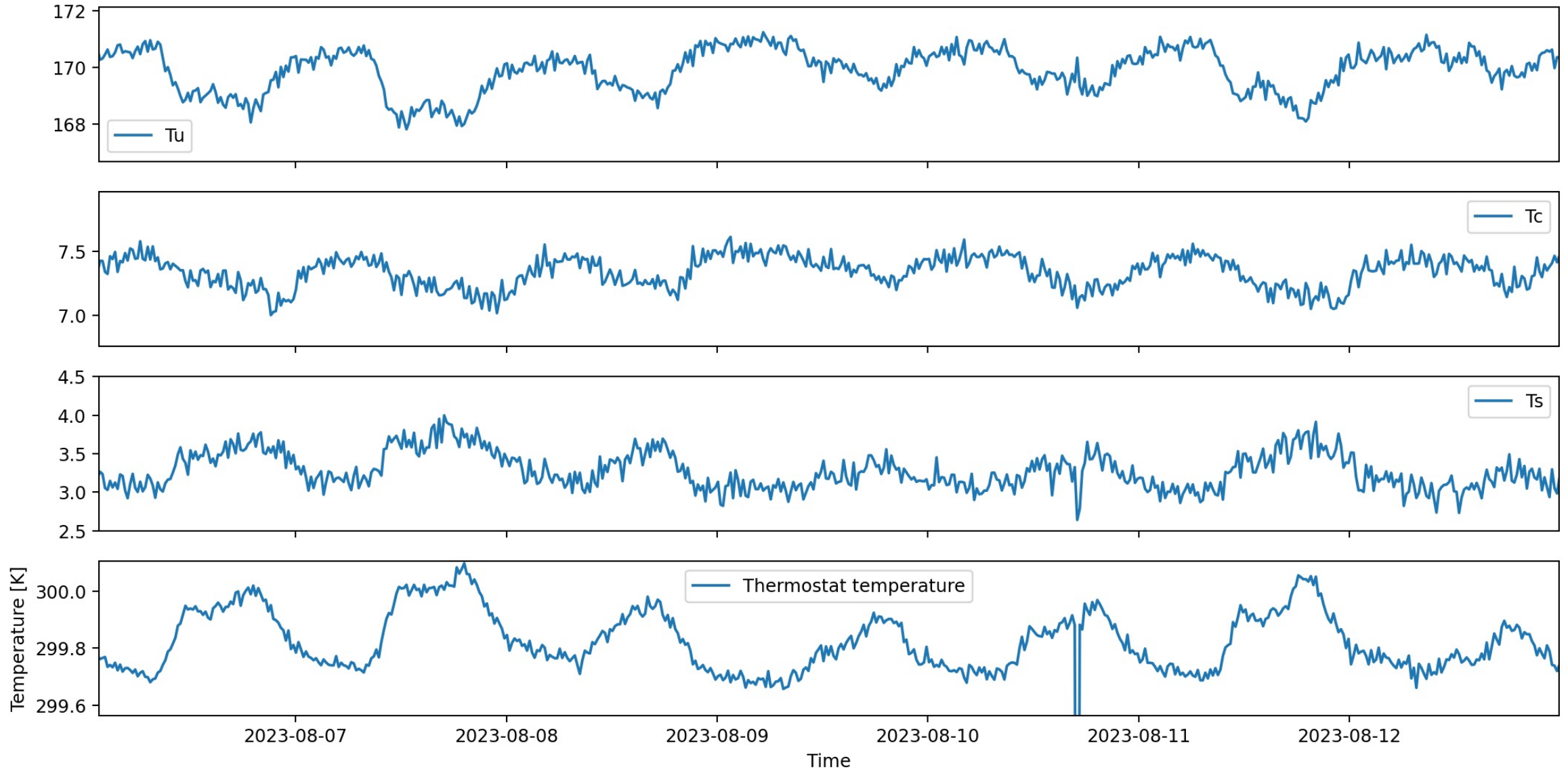
- Open
- Short
- High load
- Low Load
- Short cable

- 30KHz frequency resolution
- 25s integration time

Noise wave parameters evolution

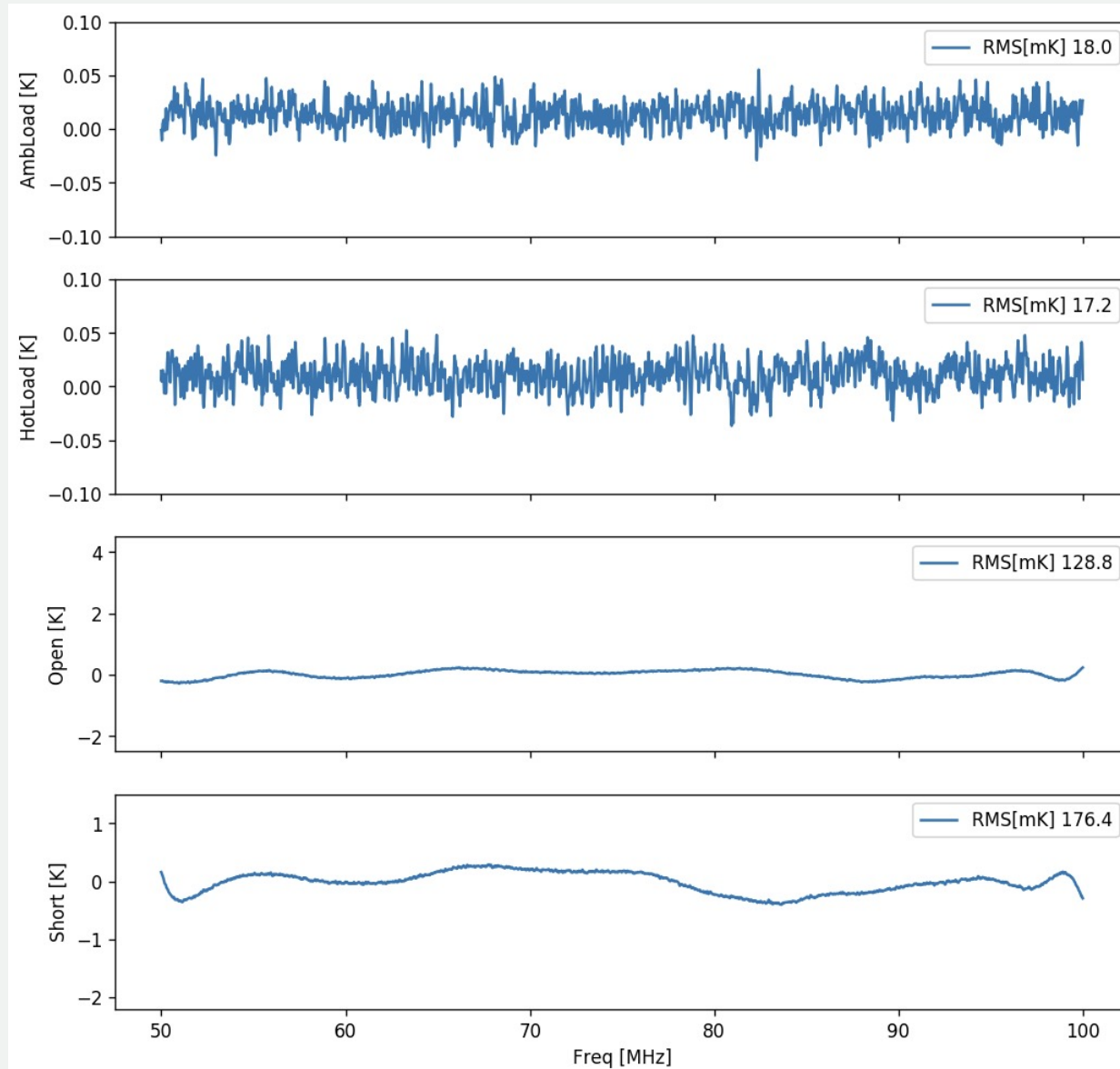
Noise parameters for different calibration periods

- 30KHz frequency resolution
- 25s integration time



Self-calibration precision

- 30KHz frequency resolution
- 13000s integration time



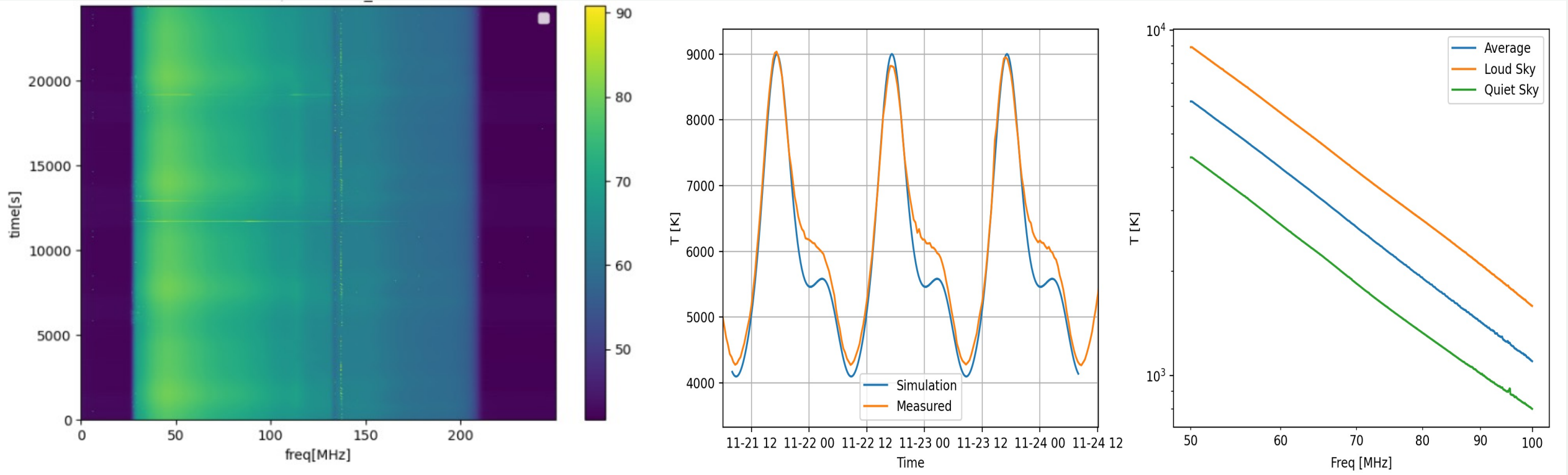
Load

Open

Short

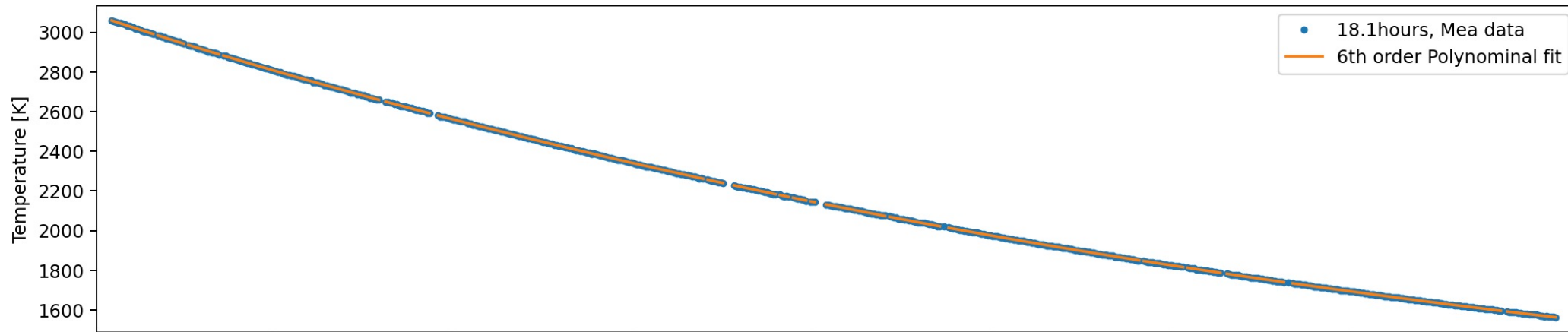
Load : $\pm 0.018K$ Open Short : $\pm 0.13K$

Sky observation

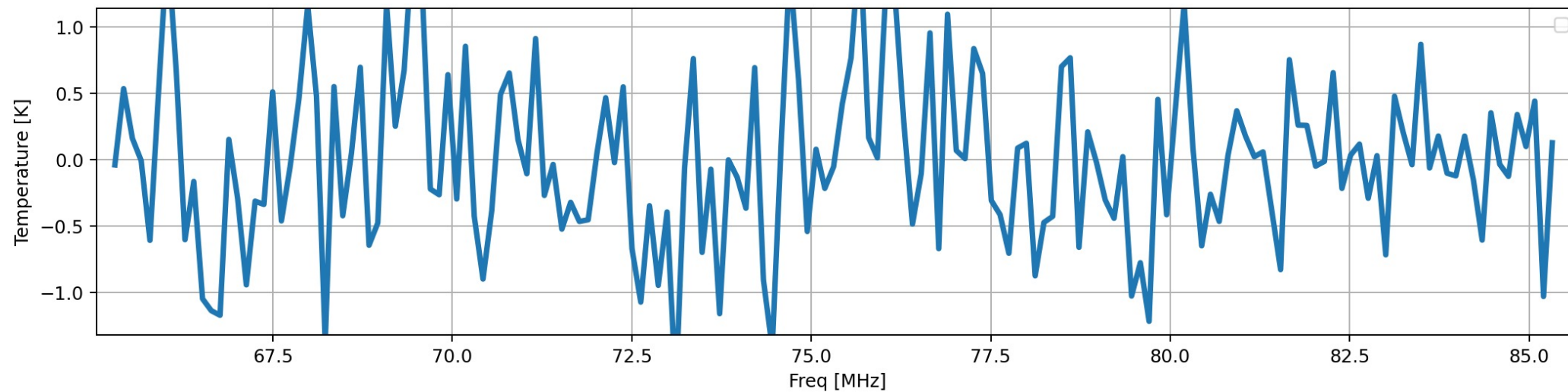


30KHz frequency resolution

Sky average spectrum (18 hours)



Spectrum



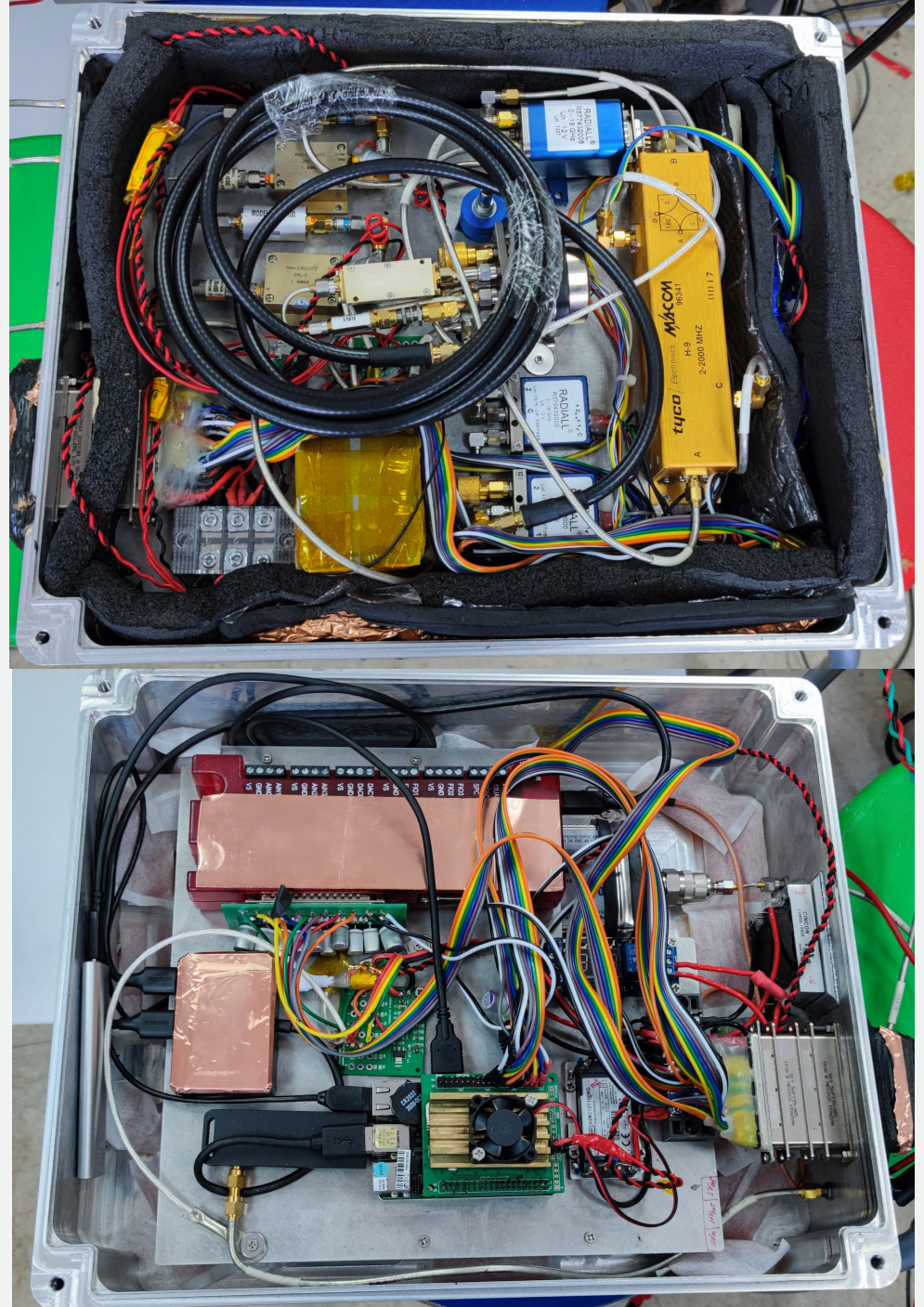
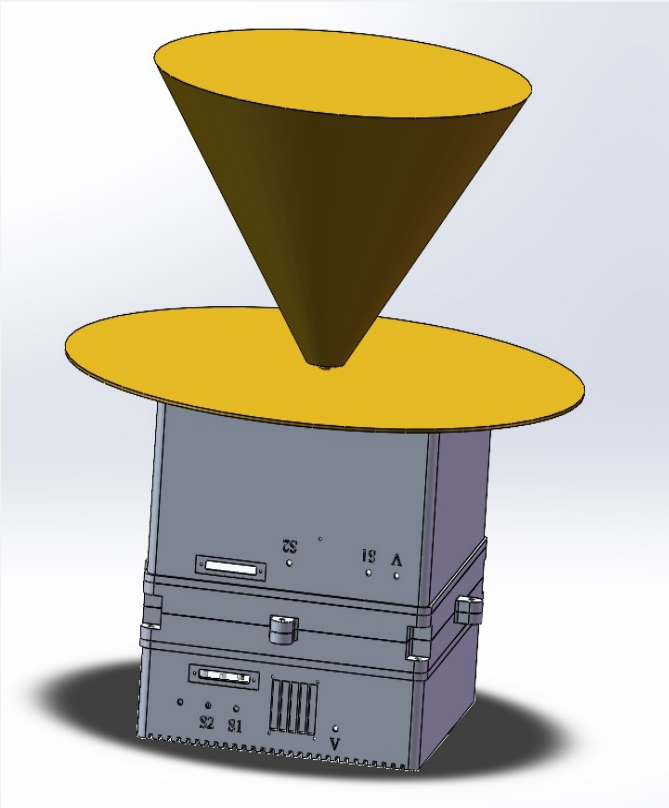
Residuals

120KHz
resolution

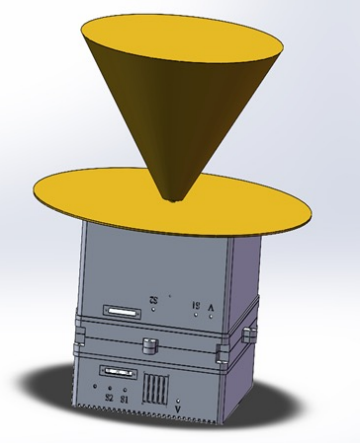
Testing of other receiver channel



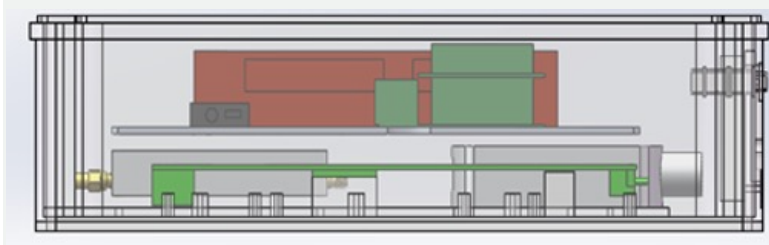
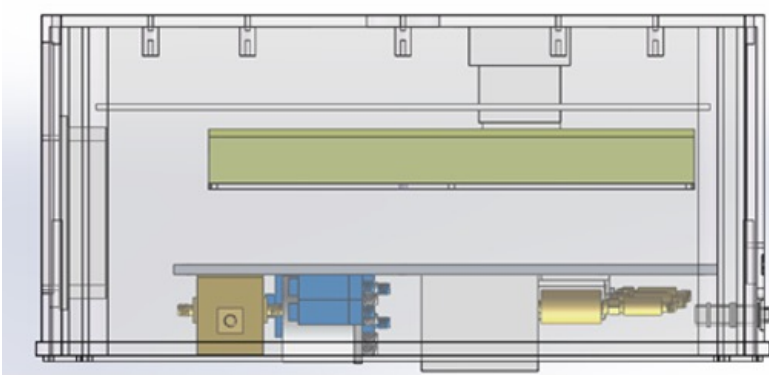
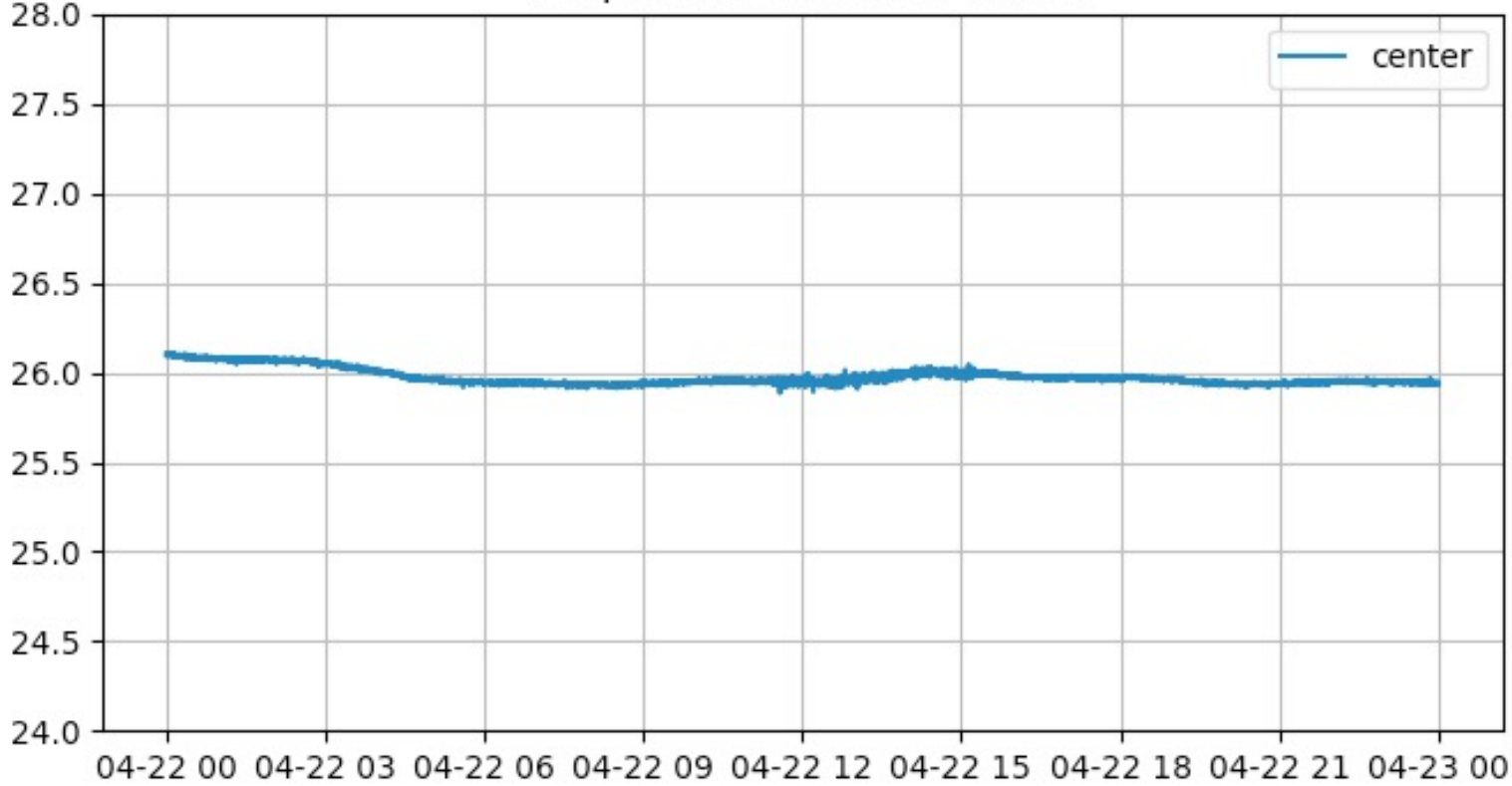
- **Prototype**



Temperature variation of key components

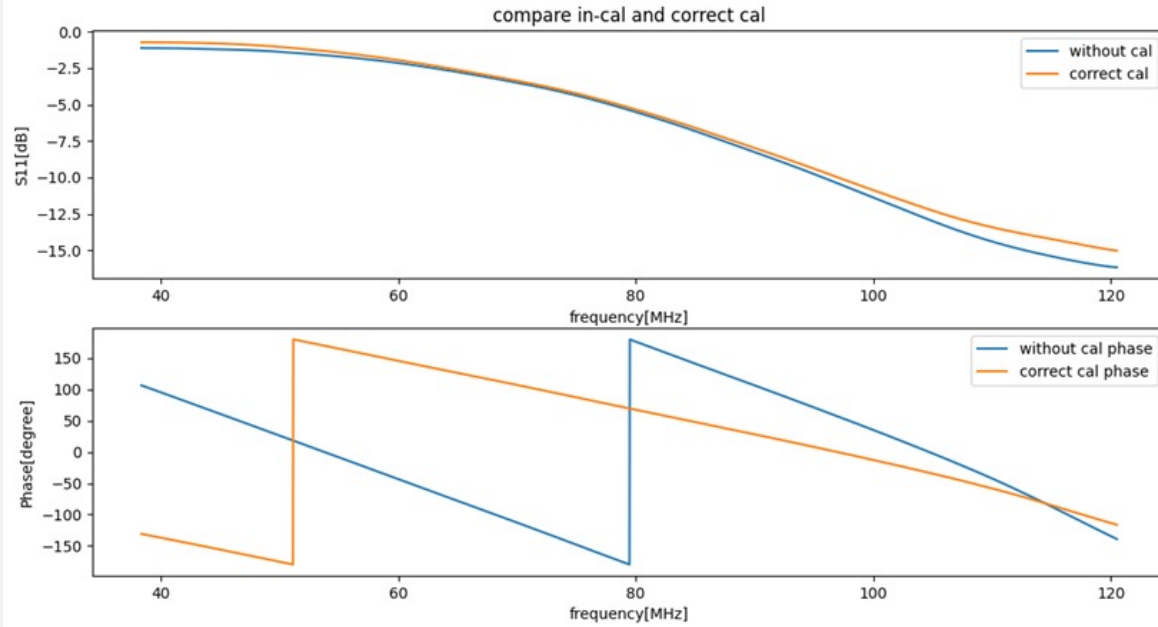


temperature at center of box

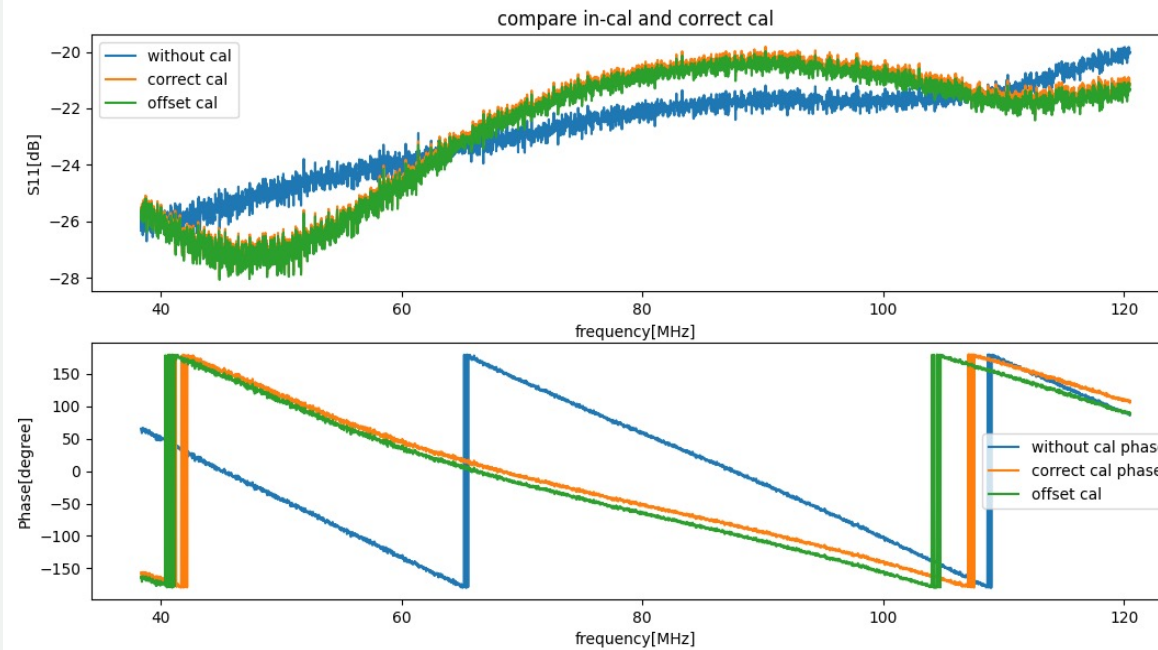


S11 of antenna and receiver

Antenna



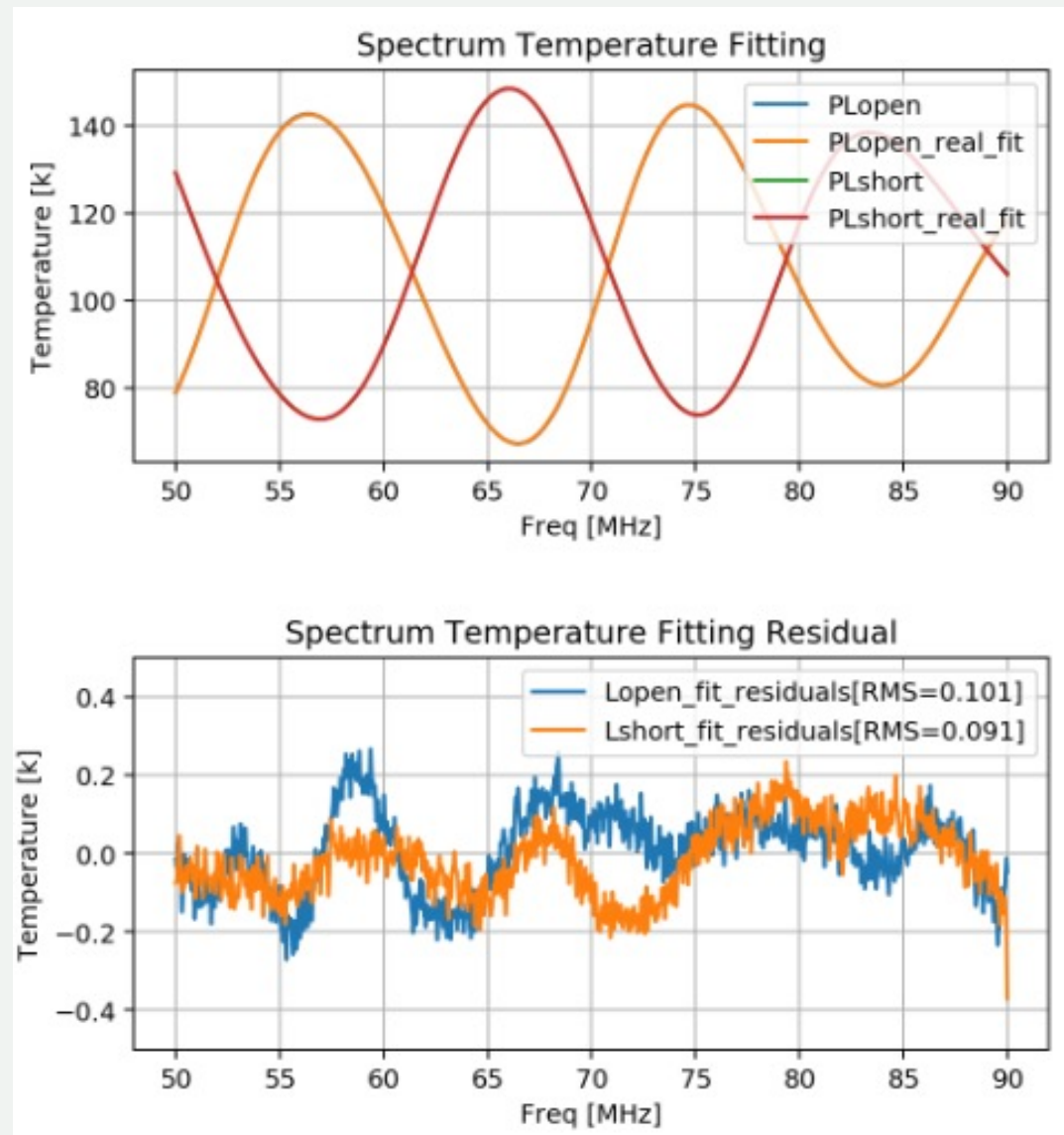
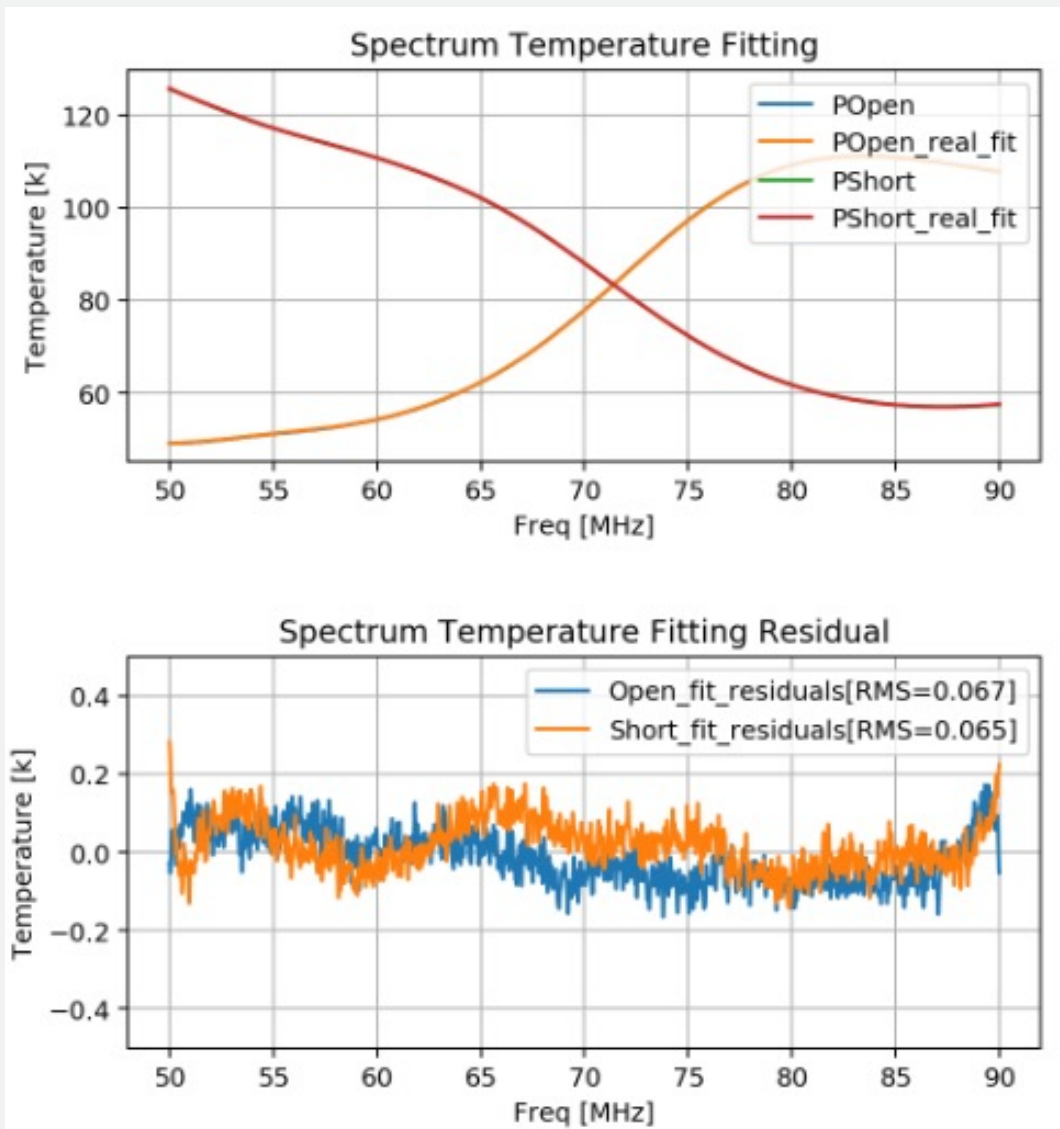
Receiver



Noise wave parameters calculation

Open, Short Spectrum and fitting residual

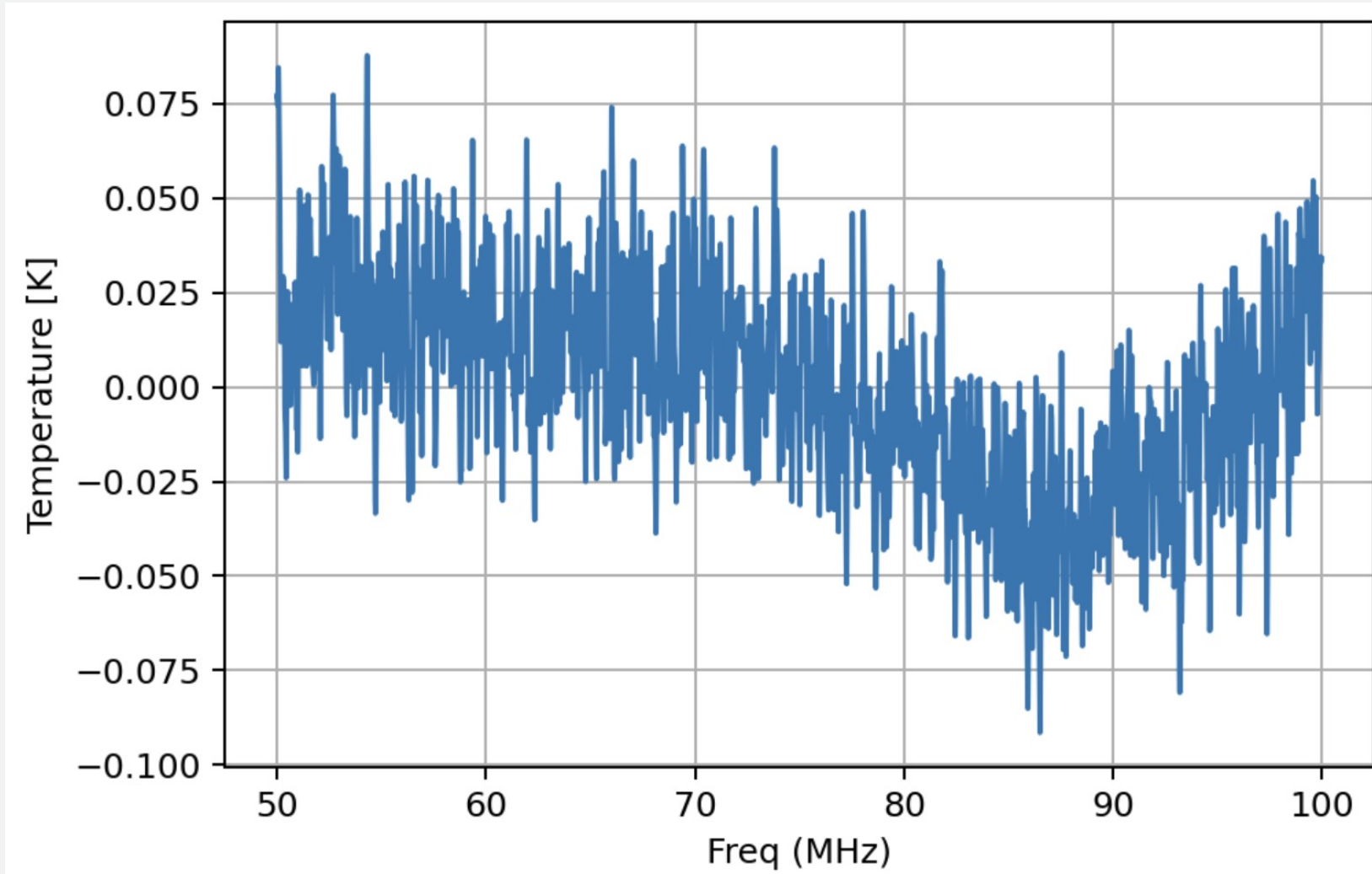
5m + Open, 5m + Short Spectrum and fitting residual



7.63KHz frequency resolution, 12000s integration time

calibration residuals of antenna simulator

50 Ohm Load as antenna simulator

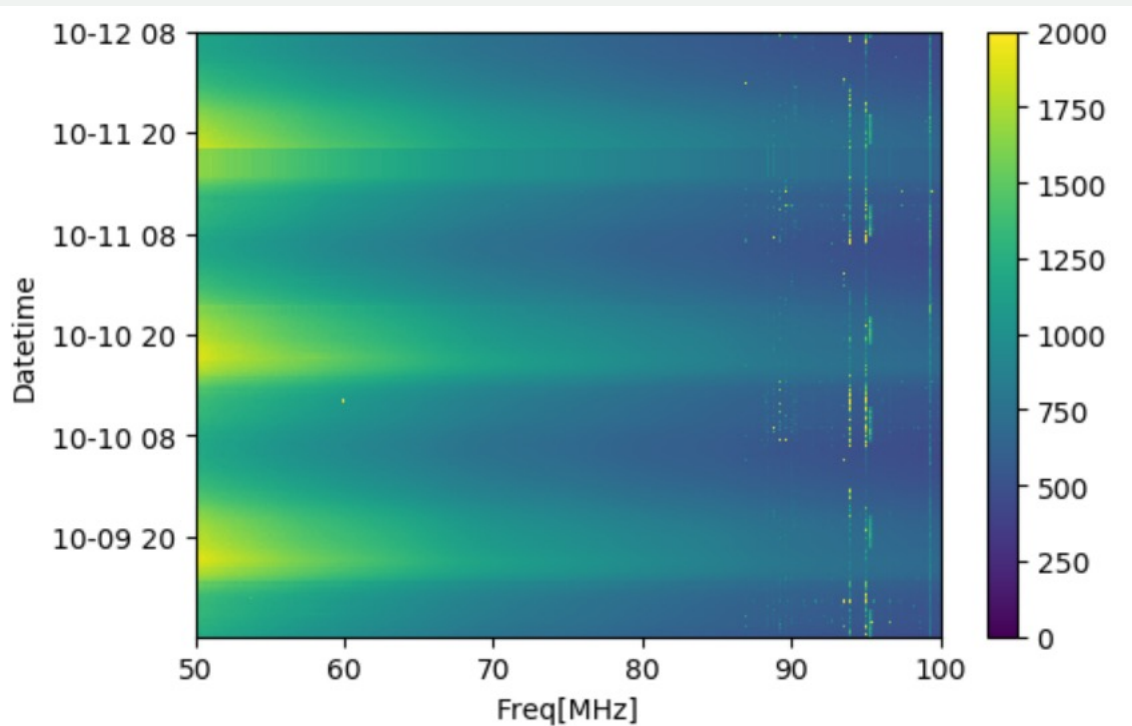


7.63KHz frequency resolution, 12000s integration time

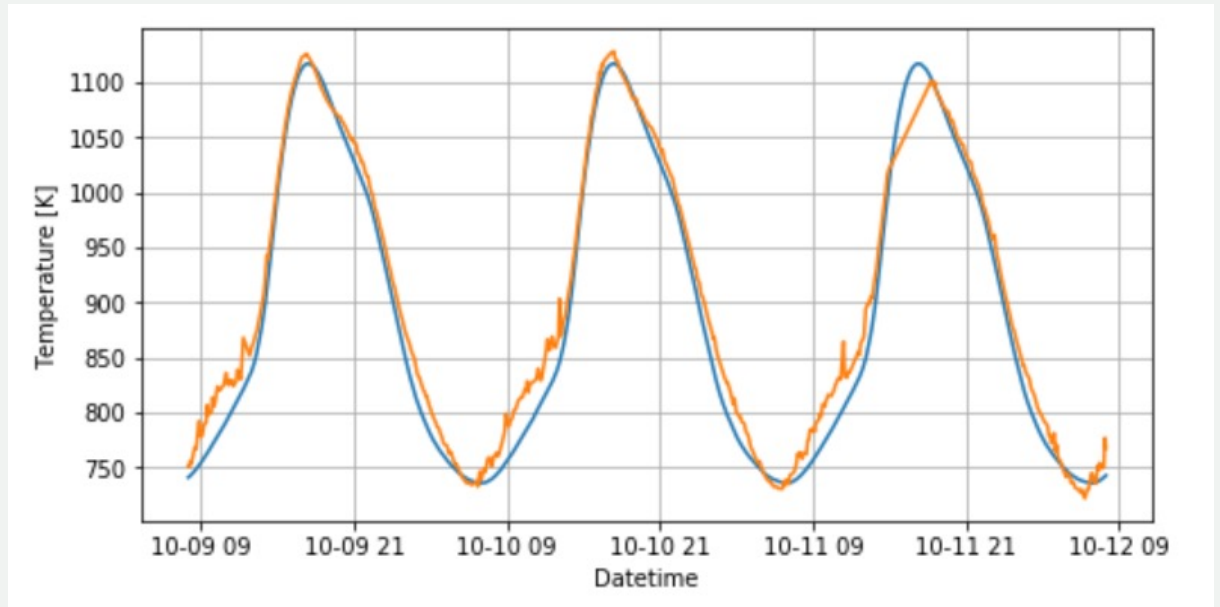
Sky observation

Sky temperature measured from
10-09 8:00 to 10-12 8:00

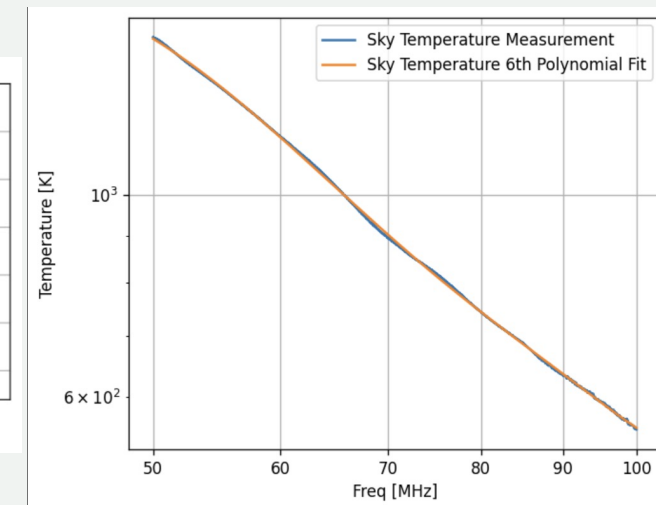
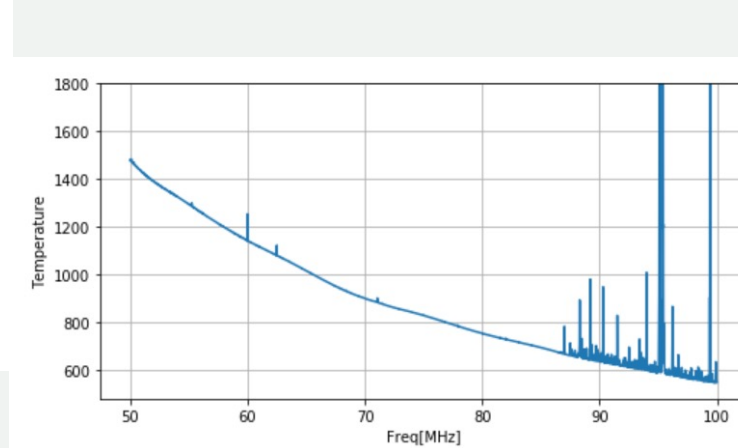
(Here we didn't consider the
radiation loss caused by soil.)



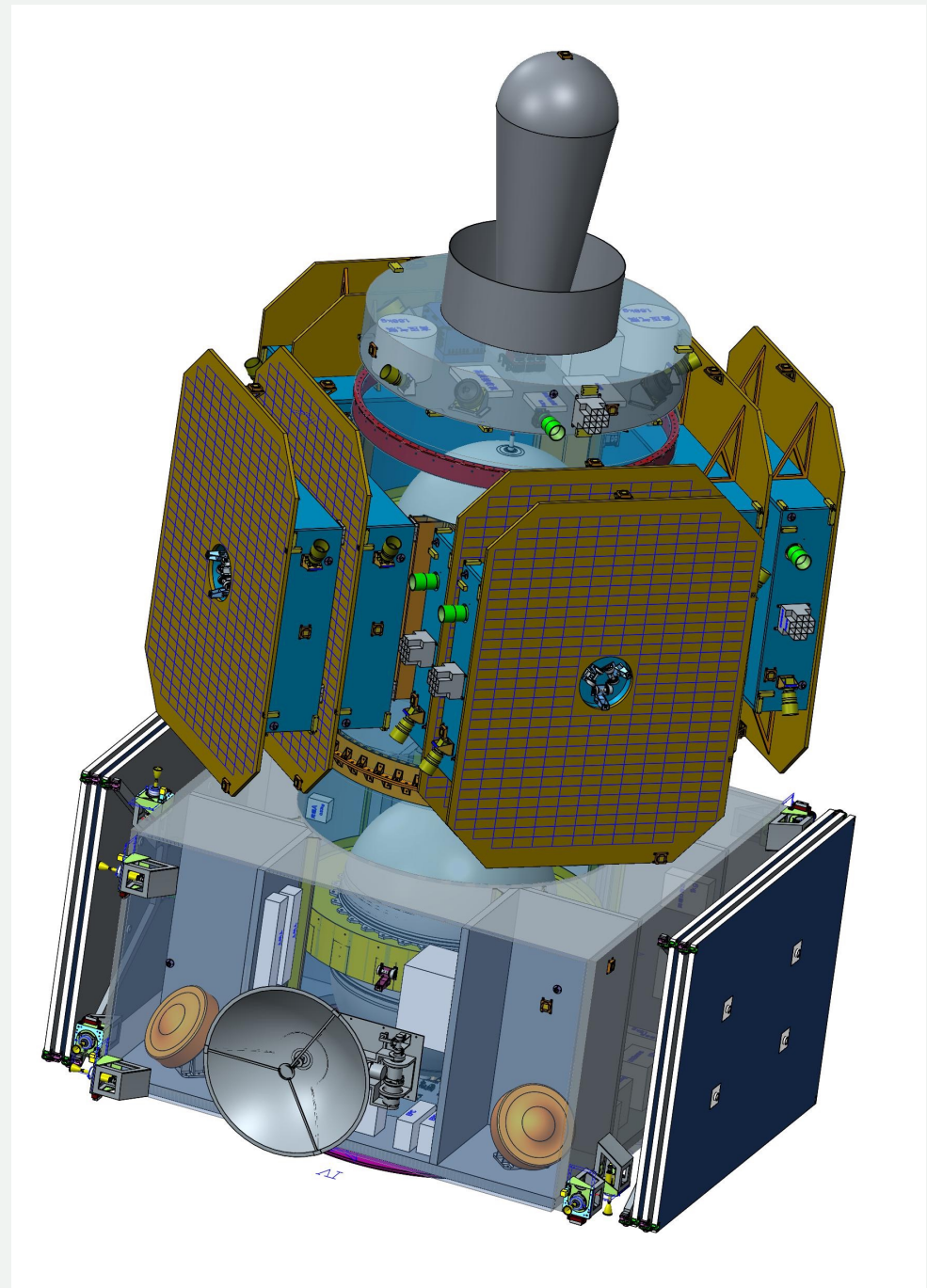
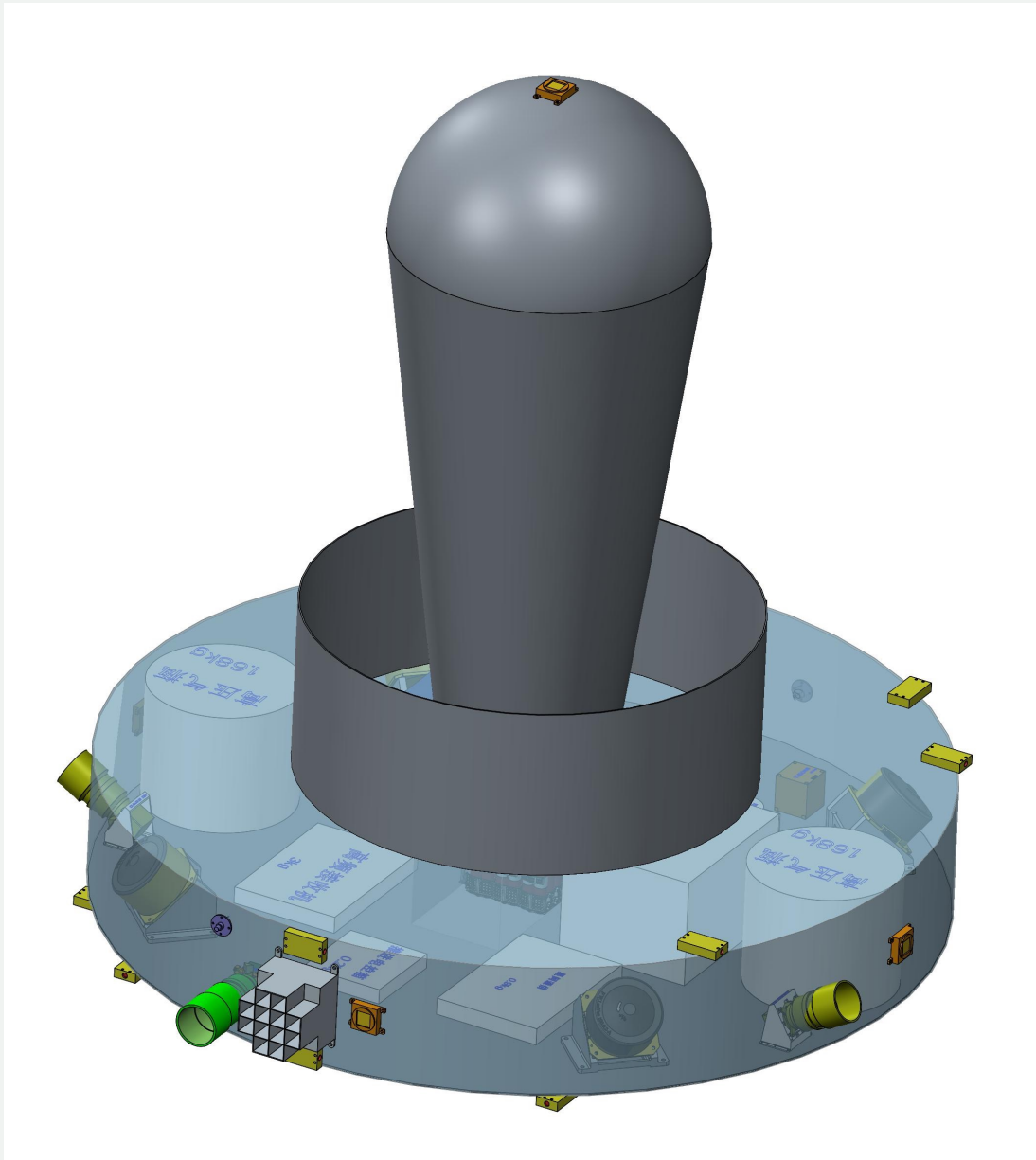
Sky temperature varies over time averaged over 50-100MHz



Sky temperature varies over time averaged over time



7.63KHz frequency resolution, 16600s observation time



Summary

- Multi-receiver design
- Antenna simulator residuals $< 0.2K$
- Field testing is still going on
- Collaboration is welcome

Thanks !

